

IPNTJ Summer School on GNSS

Theory of Precise Positioning (2) RTKLIB Practice Advanced Topics



Tokyo Univ. of Marine Science and Technology

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2014-07-28 ~ 2014-08-02 @Tokyo, Japan

Timetable

B-1 RTKLIB Introduction	July 29	8:30- 9:50
B-2 RTKLIB Practice (1)		10:10-11:30
B-3 Theory of Precise Positioning (1)		12:30-13:50
JAXA Activities & QZSS Intro by JAXA		14:10-15:30
QZSS-Demo & RTKLIB Practice (2)		15:50-17:10
B-4 Theory of Precise Positioning (2)	July 30	8:30- 9:50
B-5 Theory of RTK and RTKLIB Practice (3)		10:10-11:30
What is AIS? by JRC		12:30-12:50
Port Cruise Demo (G-1) & RTKLIB Practice (4)		12:55-14:20
Port Cruise Demo (G-2) & RTKLIB Practice (4)		14:15-15:40
B-6 Advanced Topics		15:50-17:10

B-4

Theory of Precise Positioning (2)

Time Systems

- **Time Systems**

- TAI: International Atomic Time
- UTC: Coordinated Universal Time
- Local Time (JST, EDT, ...)
- UT0, UT1, UT2: Universal Time
- GMST: Greenwich Mean Sidereal Time
- GPS Time
- GLONASS Time
- ...

Time System Conversion

TAI to UTC:

$$t_{UTC} = t_{TAI} + \text{UTC} - \text{TAI}$$

UTC to UT1:

$$t_{UT1} = t_{UTC} + \text{UT1} - \text{UTC}$$

UT1 to GMST:

$$GMST_{0h UT1} = 24110.54841 + 8640184.812866T'_u + 0.093104T'^2_u - 6.2 \times 10^{-6}T'^3_u$$

$$GMST = GMST_{0h UT1} + r(t_{UT1} - t_{0h UT1})$$

$$r = 1.002737909350795 + 5.9006 \times 10^{-11}T'_u - 5.9 \times 10^{-15}T'^2_u$$

$$T'_u = d'_u / 36525 \quad d'_u : \text{number of days elapsed since 2000 Jan 1, 12h UT1}$$

GPS Time to TAI:

$$t_{TAI} \approx t_{GPST} + 19s$$

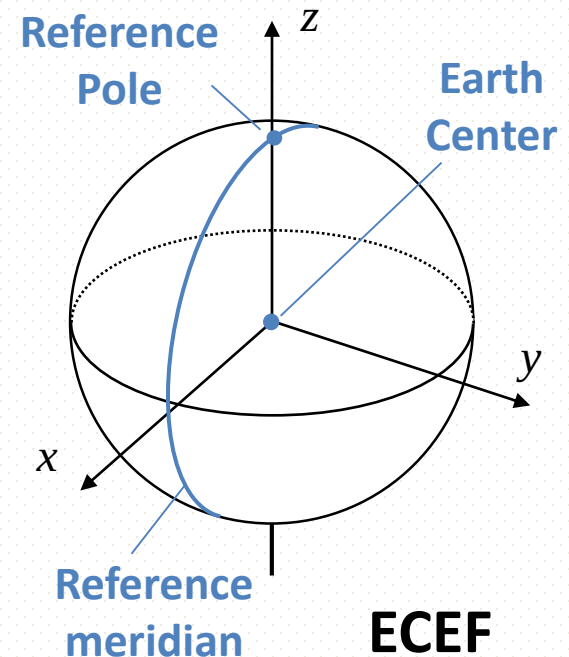
GPS Time to UTC:

$$t_{UTC} = t_{GPST} - (\Delta t_{LS} + A_0 + A_1(t_{GPST} - t_{ot}))$$

UTC-TAI (s)			
-25	1990/1/1-	-30	1996/1/1-
-26	1991/1/1-	-31	1997/7/1-
-27	1992/7/1-	-32	1999/1/1-
-28	1993/7/1-	-33	2006/1/1-
-29	1994/7/1-	-34	2009/1/1-

Coordinate Systems

- **ECEF: Earth-Centered Earth-Fixed**
 - ITRF
 - WGS 84: US (GPS)
 - PZ90: Russia (GLONASS), ...
- **ECI: Earth-Centered Inertial**
 - ICRF: International Celestial Reference Frame
- **ECI-ECEF Connection**
 - Precession/Nutation Model
 - EOP: Earth Orientation Parameters



ITRF

- **International Terrestrial Reference Frame**
 - A "Realization" of Maintained by IERS
 - GPS, VLBI, SLR, DORIS Site Position/Velocity List
 - ITRF2005, ITRF2000, ITRF97, ITRF96, ...

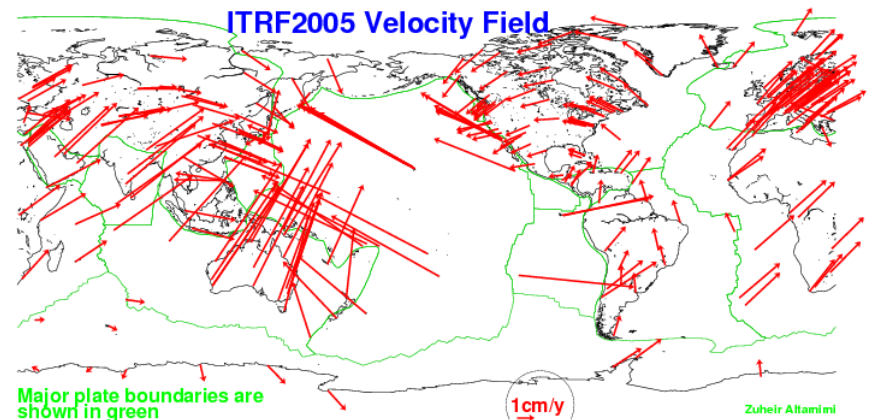
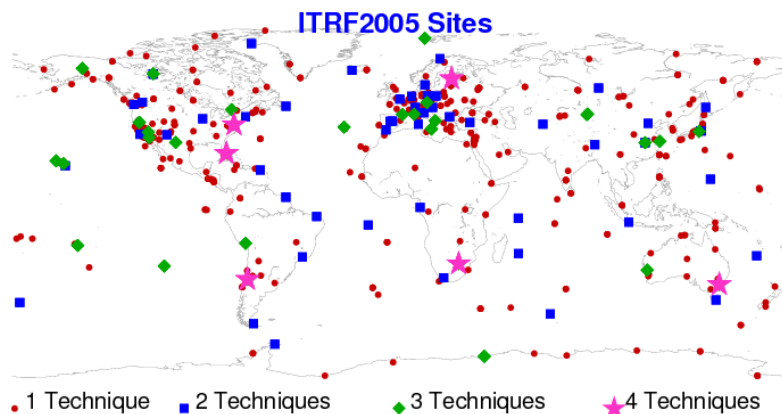
VLBI: Very Long Baseline Interferometry

SLR: Satellite Laser Ranging

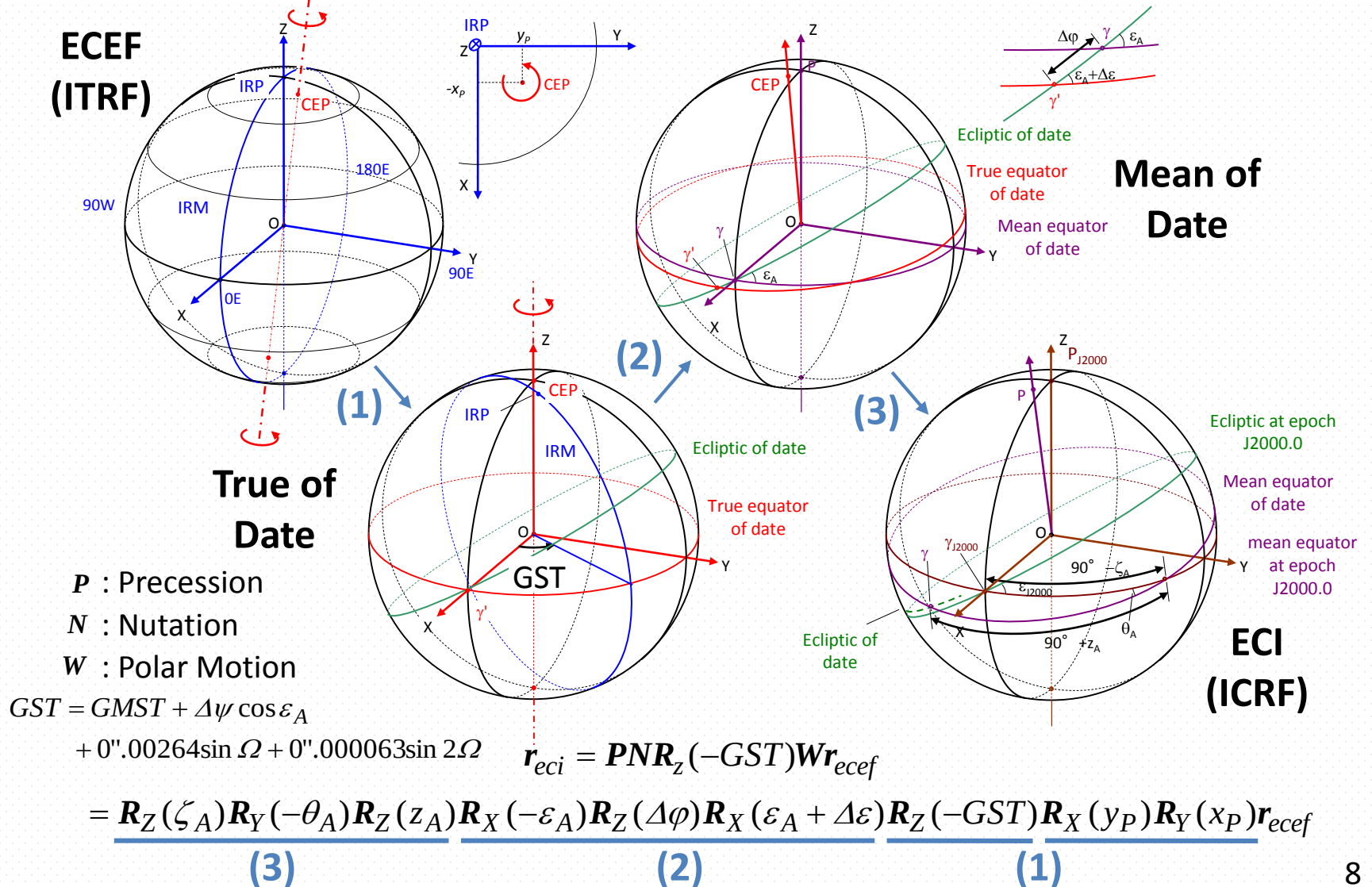
DORIS: Doppler Orbit determination and Radiopositioning Integrated on Satellite

ITRS: International Terrestrial Reference System

IERS: International Earth Rotation Service



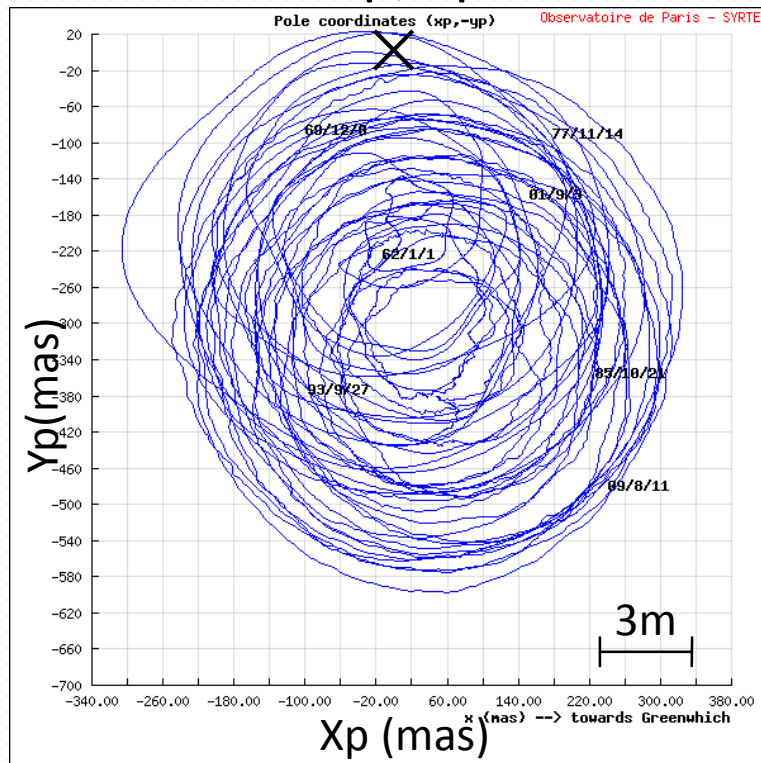
ECEF to ECI Transformation



EOP: Earth Orientation Parameters

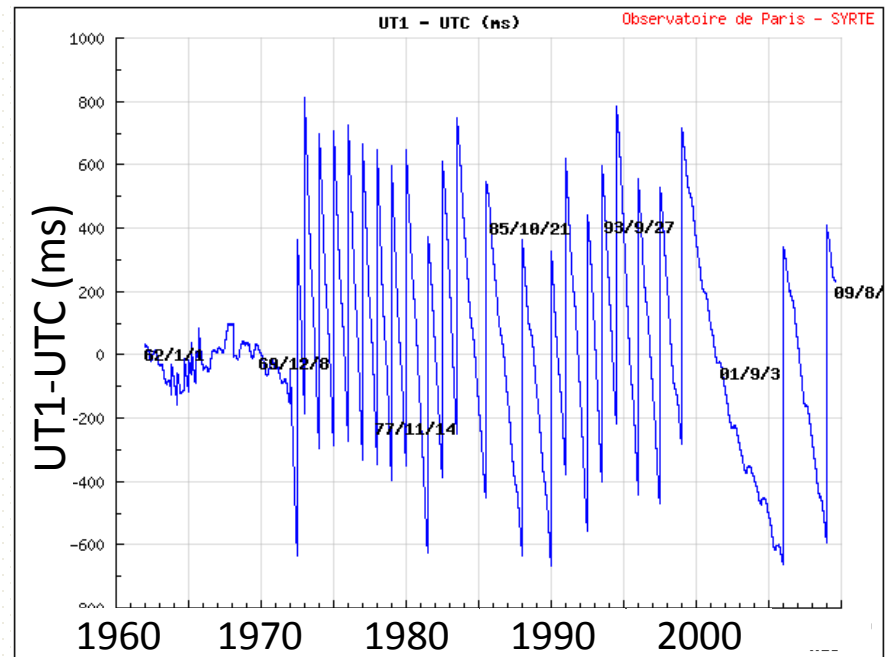
Polar Motion:

X_p, Y_p



Earth Rotation Angle:

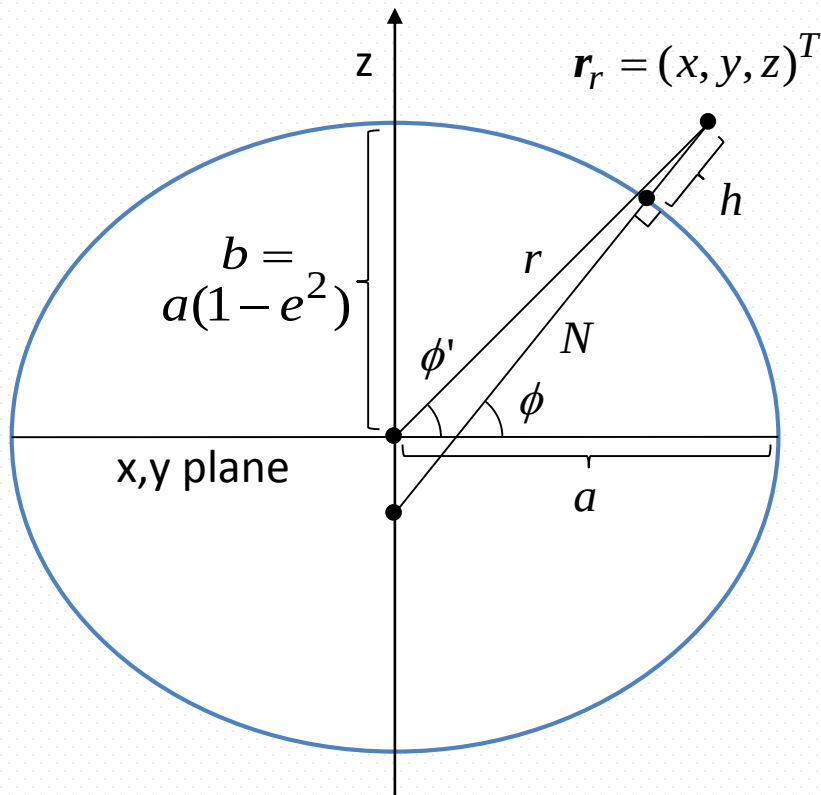
UT1-UTC



IERS C04 Series (1962/1/1-2009/8/11)

Ellipsoid and Datum

Ellipsoid:



ϕ' : Geocentric Latitude λ : Longitude
 ϕ : Geodetic Latitude h : Ellipsoidal Height

	GRS 80	WGS 84
a (m)	6378137	6378137
f	1/298.257222 101	1/298.257223 563
GM (m ³ /s ²)	3986005.000 x 10 ⁸	3986004.418 x 10 ⁸

Lat/Lon/Height to ECEF:

$$e^2 = f(2 - f)$$

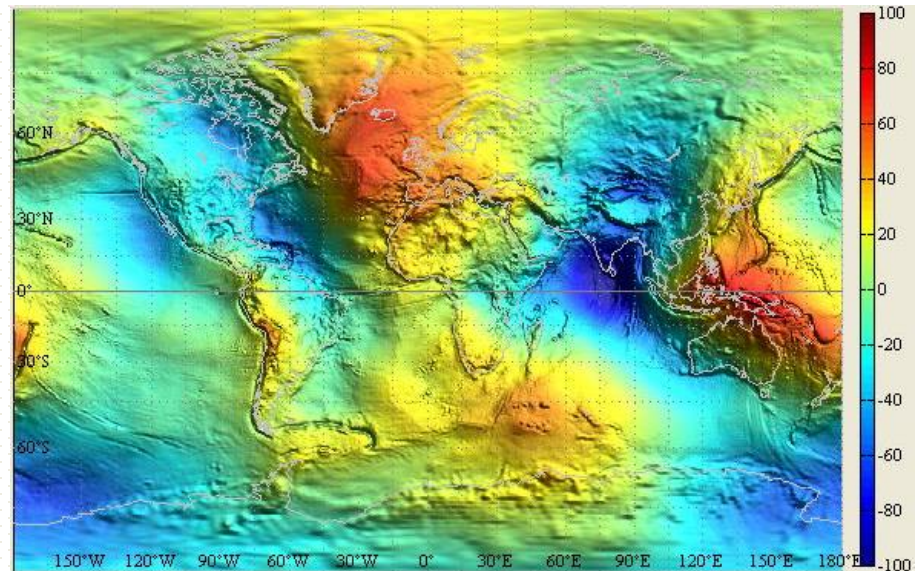
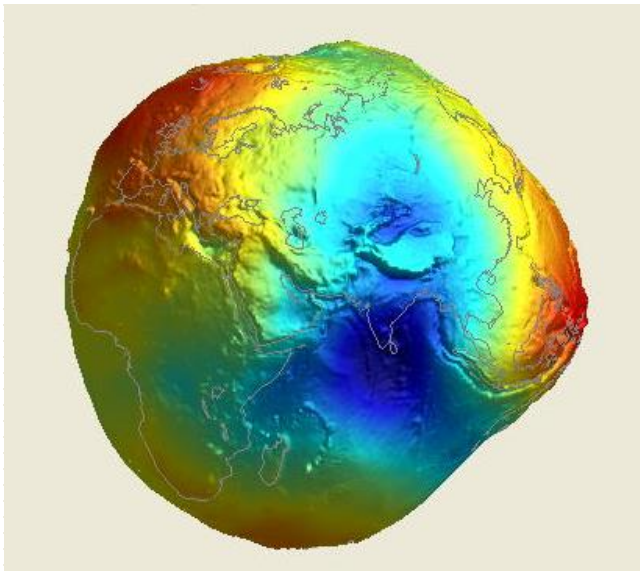
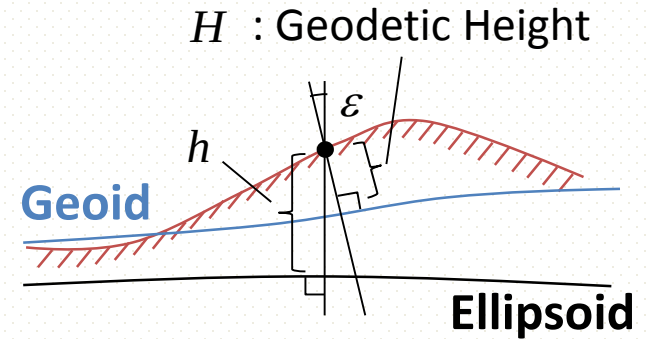
$$N = \frac{a}{\sqrt{1 - e^2 \sin^2 \phi}}$$

$$\mathbf{r}_r = \begin{pmatrix} (N + h) \cos \phi \cos \lambda \\ (N + h) \cos \phi \sin \lambda \\ (N(1 + e^2) + h) \sin \phi \end{pmatrix}$$

Geoid

Geopotential:

$$V(r, \phi', \lambda) = \frac{GM}{r} \left\{ 1 + \sum_{n=2}^{\infty} \sum_{m=0}^n \left(\frac{a}{r} \right)^n (\bar{C}_{nm} Y_{nmc} + \bar{S}_{nm} Y_{nms}) \right\}$$



EGM96 Geoid Model

Spherical Harmonics

Spherical harmonic functions:

$$Y_{n0} = Y_{n0c}$$

$$Y_{nmc} = \bar{P}_{nm}(\sin \phi') \cos m\lambda$$

$$Y_{nms} = \bar{P}_{nm}(\sin \phi') \sin m\lambda$$

Legendre function:

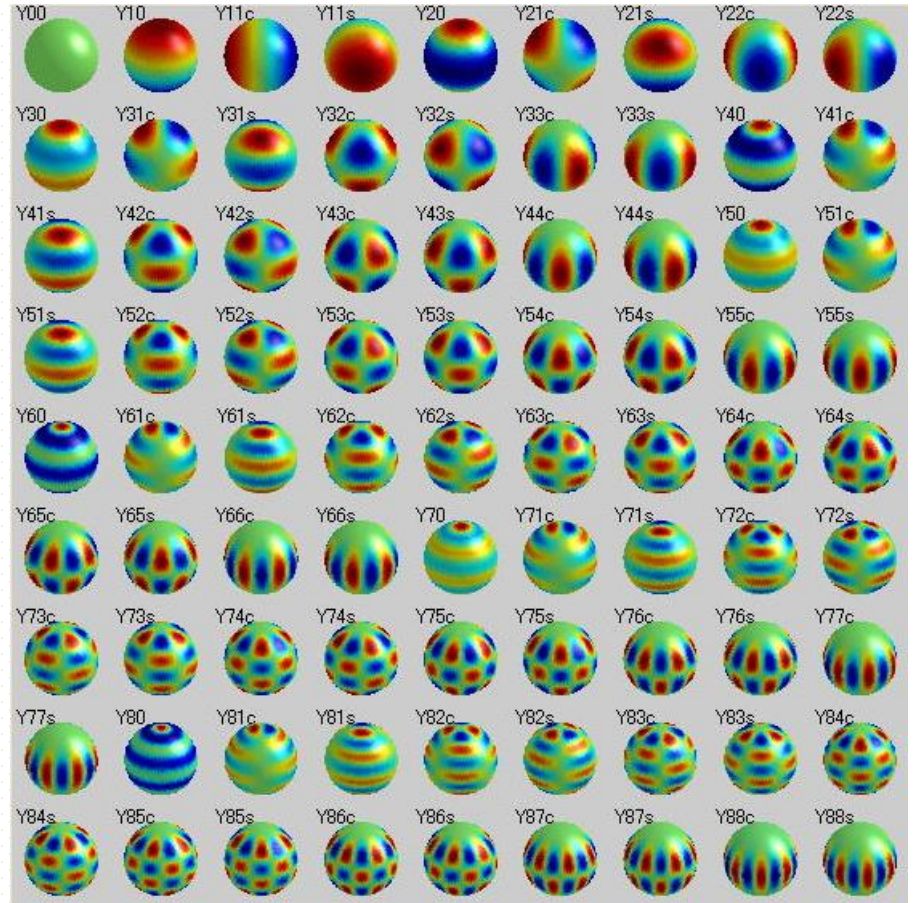
$$\bar{P}_{nm} = N_{nm} P_{nm}, P_{00}(x) = 1, P_{10}(x) = x$$

$$P_{n-1,n}(x) = 0,$$

$$P_{nn}(x) = (2n-1)(1-x^2)^{1/2} P_{n-1,n-1}(x)$$

$$P_{nm}(x) = \frac{(2n-1)xP_{n-1,m}(x) - (n+m-1)P_{n-2,m}(x)}{n-m}$$

$$N_{nm} = \begin{cases} \sqrt{2n+1} & (m=0) \\ \sqrt{\frac{2(2n+1)(n-m)!}{(n+m)!}} & (m>0) \end{cases}$$



Coordinates Transformation

Helmert Transformation (A to B):

$$\begin{pmatrix} x \\ y \\ z \end{pmatrix}_B = \begin{pmatrix} T_1 \\ T_2 \\ T_3 \end{pmatrix} + (1 + D) \begin{pmatrix} 1 & -R_3 & R_2 \\ R_3 & 1 & -R_1 \\ -R_2 & R_1 & 1 \end{pmatrix} \begin{pmatrix} x \\ y \\ z \end{pmatrix}_A$$

- T1, T2, T3 : Translation along coordinate axis
- D : Scale factor
- R1, R2, R3 : Rotation of coordinate axis

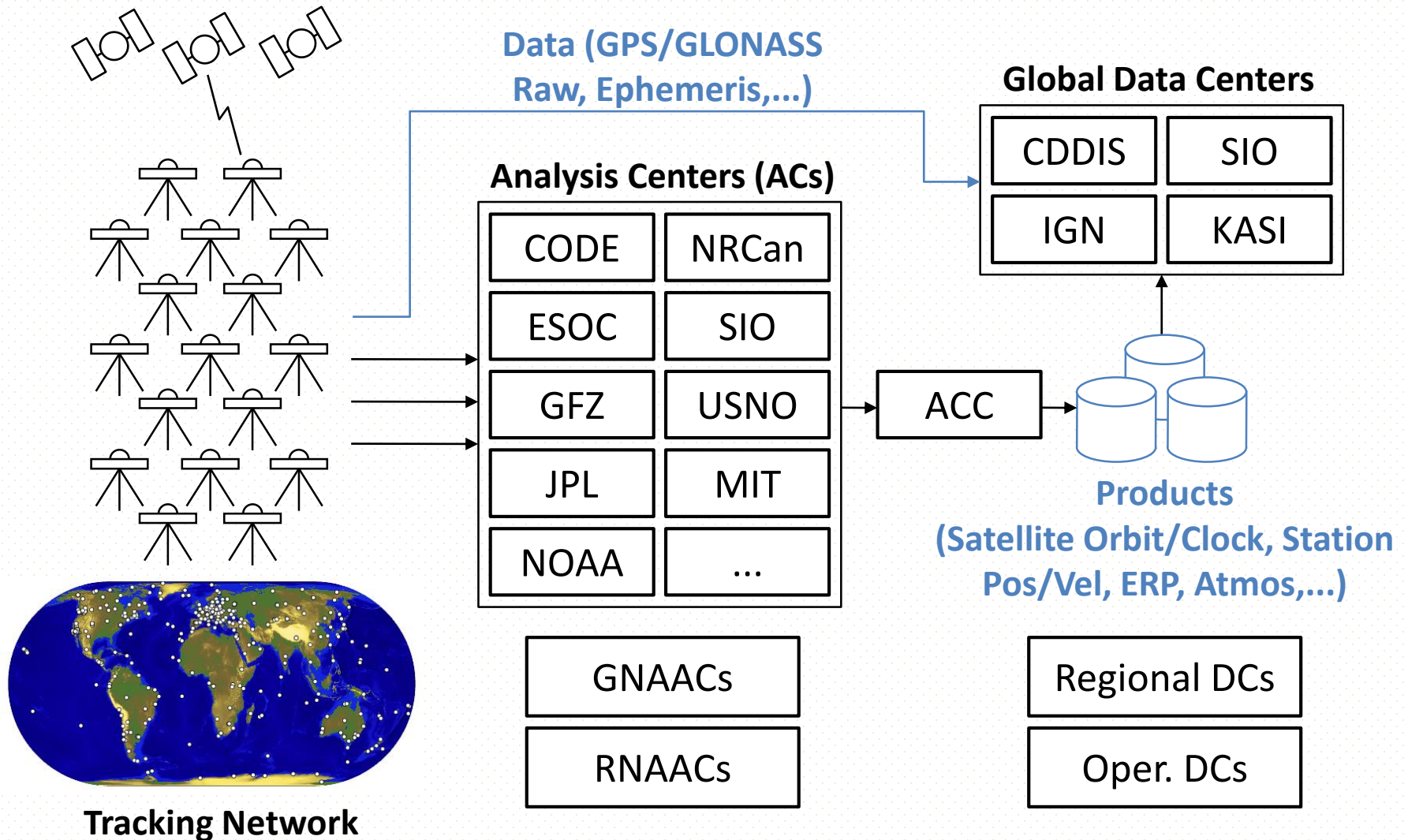
Coordinates		T1	T2	T3	D	R1	R2	R3
A	B	(mm)	(mm)	(mm)	(10 ⁻⁹)	(mas)	(mas)	(mas)
ITRF2005	ITRF2000	0.1	-0.8	-5.8	0.40	0.00	0.00	0.00
		-0.2/y	0.1/y	-1.8/y	0.08/y	0.00/y	0.00/y	0.00/y

(Epoch 2000.0)

Precise Ephemeris

- **Precise Satellite Orbit and Clock**
 - By Post-Processing or in Real-time
 - Observation Data of Tracking Stations World-Wide
- **Format:**
 - Orbit: NGS SP3
 - Clock: NGS SP3 or RINEX Clock Extension
- **Contents:**
 - Orbit: ECEF-Positions of Satellite Mass Center
 - Clock: Clock-biases wrt Time Scale Aligned to GPS Time

IGS: International GNSS Service



IGS Products

		Final (IGS)	Rapid (IGR)	Ultra-Rapid (IGU)		Broadcast
				Observed	Predicted	
Accuracy	Orbit	~2.5cm	~2.5cm	~3cm	~5cm	~100cm
	Clock	~75ps RMS ~20ps STD	~75ps RMS ~25ps STD	~150ps RMS ~50ps STD	~3ns RMS ~1.5ns STD	~5ns RMS ~2.5ns STD
Latency		12-18 days	17-41 hours	3-9 hours	realtime	realtime
Updates		every Thursday	at 17 UTC daily	at 03, 09, 15, 21 UTC	at 03, 09, 15, 21 UTC	-
Sample Interval	Orbit	15min	15min	15min	15min	daily
	Clock	Sat: 30s Stn: 5min	5min	15min	15min	daily

(2009/8, <http://igsceb.jpl.nasa.gov/>)

Interpolation of Satellite Orbit

Lagrange Interpolation:

$$\begin{aligned} \mathbf{r}^s(t) = & \frac{(t-t_2)(t-t_3)\dots(t-t_{n+1})}{(t_1-t_2)(t_1-t_3)\dots(t_1-t_{n+1})} \mathbf{r}^s(t_1) + \frac{(t-t_1)(t-t_3)\dots(t-t_{n+1})}{(t_2-t_1)(t_2-t_3)\dots(t_2-t_{n+1})} \mathbf{r}^s(t_2) \\ & + \frac{(t-t_1)(t-t_2)\dots(t-t_{n+1})}{(t_3-t_1)(t_3-t_2)\dots(t_3-t_{n+1})} \mathbf{r}^s(t_3) + \dots + \frac{(t-t_1)(t-t_2)\dots(t-t_n)}{(t_{n+1}-t_1)(t_{n+1}-t_2)\dots(t_{n+1}-t_n)} \mathbf{r}^s(t_{n+1}) \end{aligned}$$

Interpolation Error of 15-min Sample Orbit

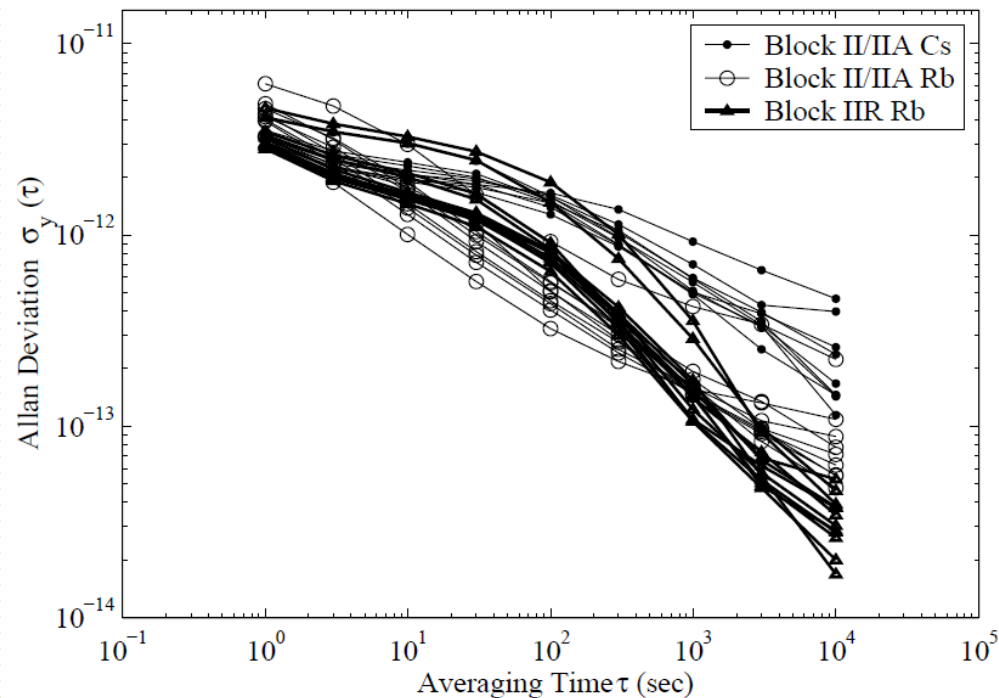
Degree of Polynomial	Position RMS Error (cm)			Velocity RMS Error (cm/s)		
	Radial	Along-Trk	Cross-Trk	Radial	Along-Trk	Cross-Trk
n=5	72.10	73.84	57.48	0.253	0.260	0.202
n=6	7.31	6.89	5.75	0.032	0.031	0.025
n=7	0.63	0.63	0.50	0.017	0.019	0.014
n=8	0.08	0.11	0.08	0.017	0.018	0.013
n=9	0.05	0.11	0.05	0.017	0.018	0.013
n=10	0.05	0.10	0.06	0.017	0.018	0.013
n=11	0.05	0.12	0.06	0.017	0.018	0.013

Interpolation of Satellite Clock

Linear Interpolation:

$$dT^s(t) = \frac{(t_2 - t)dT^s(t_1) + (t - t_1)dT^s(t_2)}{t_2 - t_1} + \Delta t_{rel}$$

Satellite Clock Stability:



Ionospheric Delay

Ionospheric Delay Model:

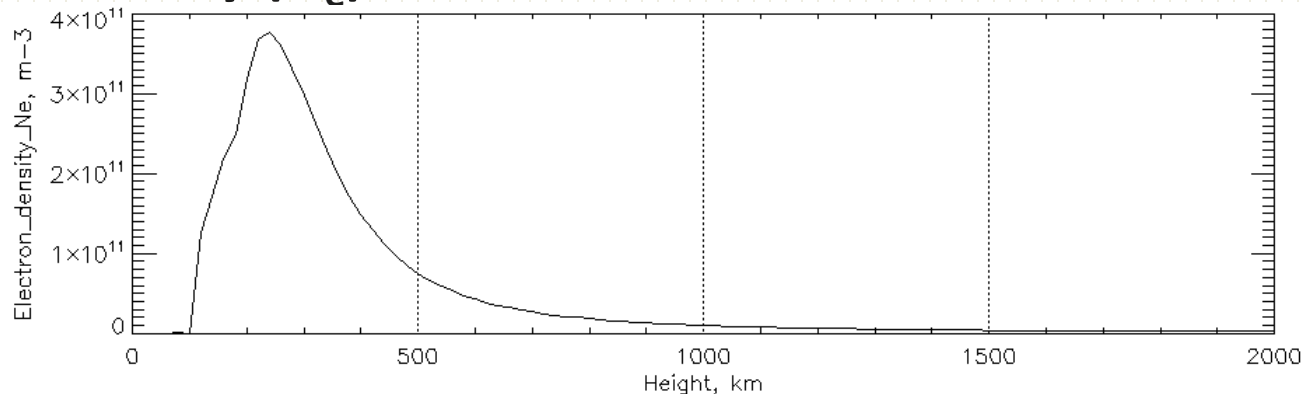
$$n^2 = 1 - \frac{X}{1 - iZ - \frac{Y_T^2}{2(1 - X - iZ)} \pm \sqrt{\frac{Y_T^4}{4(1 - X - iZ)^2} + Y_L^2}} \approx 1 - X = 1 - f_N^2 / f^2 \text{ (L-band)}$$

: Appleton-Hartree Formula

$$n = \sqrt{1 - f_N^2 / f^2} \approx 1 - f_N^2 / 2f^2 = 1 - 40.30N_e / f^2 \quad f_N^2 = \frac{N_e e^2}{4\pi^2 \epsilon_0 m_e} : \text{plasma frequency}$$

$$I_r^S \approx \int 40.30N_e / f^2 dl = 40.30 \times 10^{16} \text{TEC} / f^2 \quad \text{TEC: Total Electron Content}$$

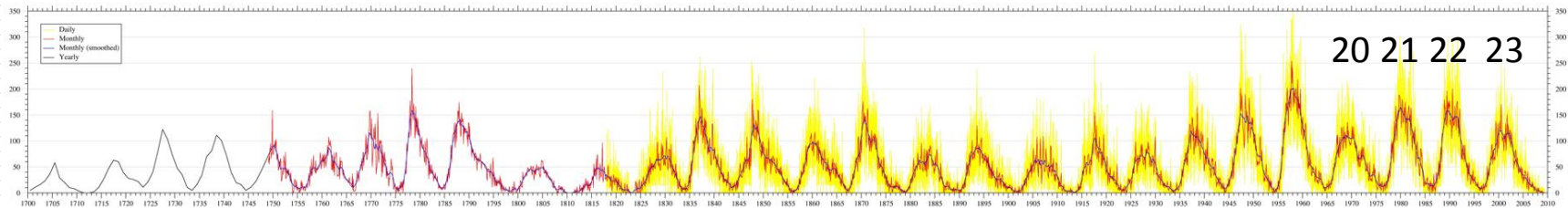
Electron Density (N_e):



IRI-2007 model: 2009/7/31 0:00 Tokyo (<http://modelweb.gsfc.nasa.gov/models/iri.html>)

Solar Cycle

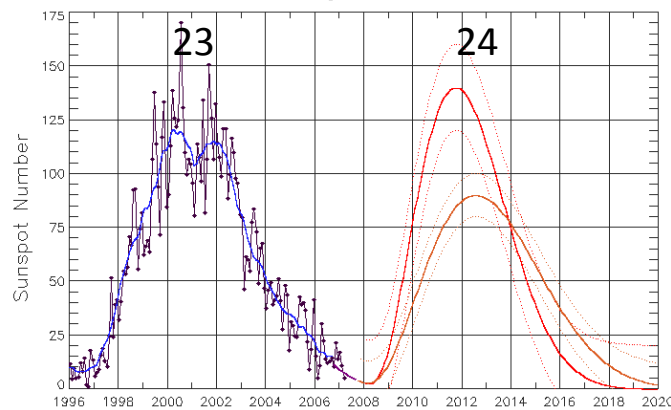
International Sunspot Number (ISN): 1700-2009



by SIDC (Solar Influences Data Analysis Center) in Belgium (<http://sidc.oma.be>)

Solar Cycle Prediction: Cycle 24

Solar Cycle 24 Sunspot Number Prediction
Data Through 31 Mar 07

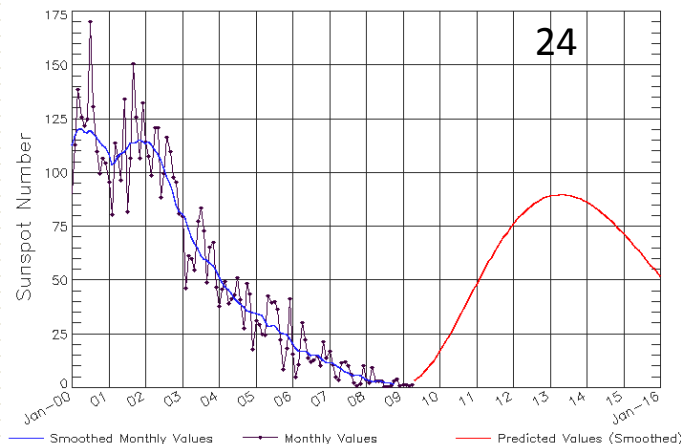


Low Prediction (Smoothed) High Prediction (Smoothed) 1-Sigma Error
Smoothed Monthly Values Monthly Values

Updated 2007 Apr 20

NOAA/SEC Boulder, CO USA Updated 2008 May 08

ISES Solar Cycle Sunspot Number Progression
Data Through Apr 09



Smoothed Monthly Values Monthly Values Predicted Values (Smoothed)

NOAA/SWPC Boulder, CO USA

by NOAA SWPC (Space Weather Prediction Center) (<http://www.swpc.noaa.gov/SolarCycle>)

LC: Linear Combination

$$C = a\Phi_1 + b\Phi_2 + cP_1 + dP_2 (\Phi_1 = \lambda_1\phi_1, \Phi_2 = \lambda_2\phi_2)$$

	LC	Coefficients				Wave Length (cm)	Ionos Effect wrt L1	Typical Noise (cm)
		a	b	c	d			
L1	L1 Carrier-Phase	1	0	0	0	19.0	1.0	0.3
L2	L2 Carrier-Phase	0	1	0	0	24.4	1.6	0.3
LC/L3	Iono-Free Phase	C_1	C_2	0	0	-	0.0	0.9
LG/L4	Geometry-Free Phase	1	-1	0	0	-	0.6	0.4
WL	Wide-Lane Phase	λ_W / λ_1	$-\lambda_W / \lambda_2$	0	0	86.2	1.3	1.7
NL	Narrow-Lane Phase	λ_N / λ_1	λ_N / λ_2	0	0	10.7	1.3	1.7
MW	Melbourne-Wübbena	λ_W / λ_1	$-\lambda_W / \lambda_2$	λ_N / λ_1	λ_N / λ_2	86.2	0.0	21
MP1	L1-Multipath	$2C_2 - 1$	$-2C_2$	1	0	-	0.0	30
MP2	L2-Multipath	$-2C_1$	$2C_1 - 1$	0	1	-	0.0	30

$$C_1 = f_1^2 / (f_1^2 - f_2^2), C_2 = -f_2^2 / (f_1^2 - f_2^2), \lambda_W = 1 / (1/\lambda_1 - 1/\lambda_2), \lambda_N = 1 / (1/\lambda_1 + 1/\lambda_2)$$

Single Layer Model

Ionospheric Delay Model:

$$I = \frac{40.30 \times 10^{16}}{f^2} TEC \approx \frac{1}{\cos z'} \frac{40.30 \times 10^{16}}{f^2} \times VTEC(t, \phi_{pp}, \lambda_{pp})$$

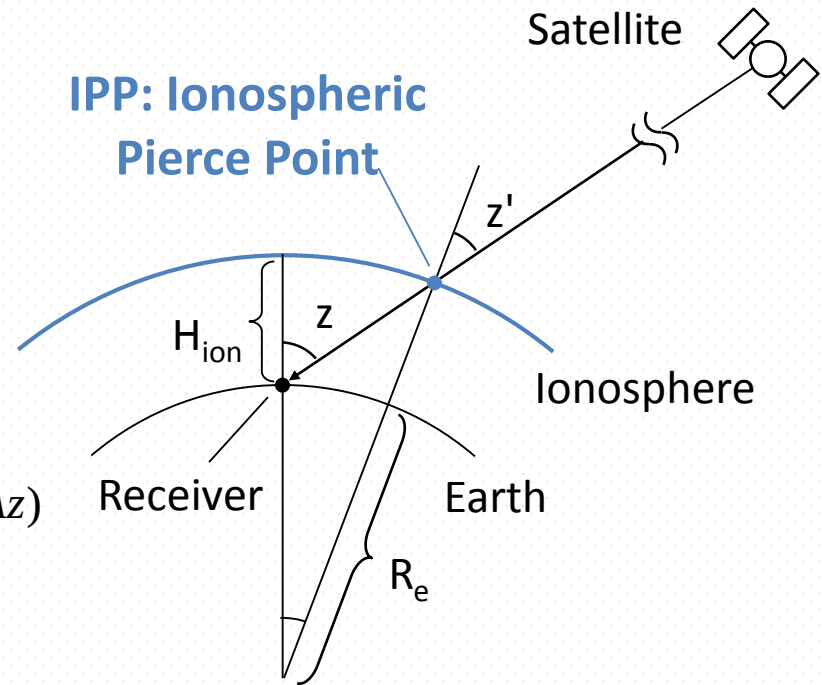
IPP Position/Slant Factor:

$$z = \pi/2 - El$$

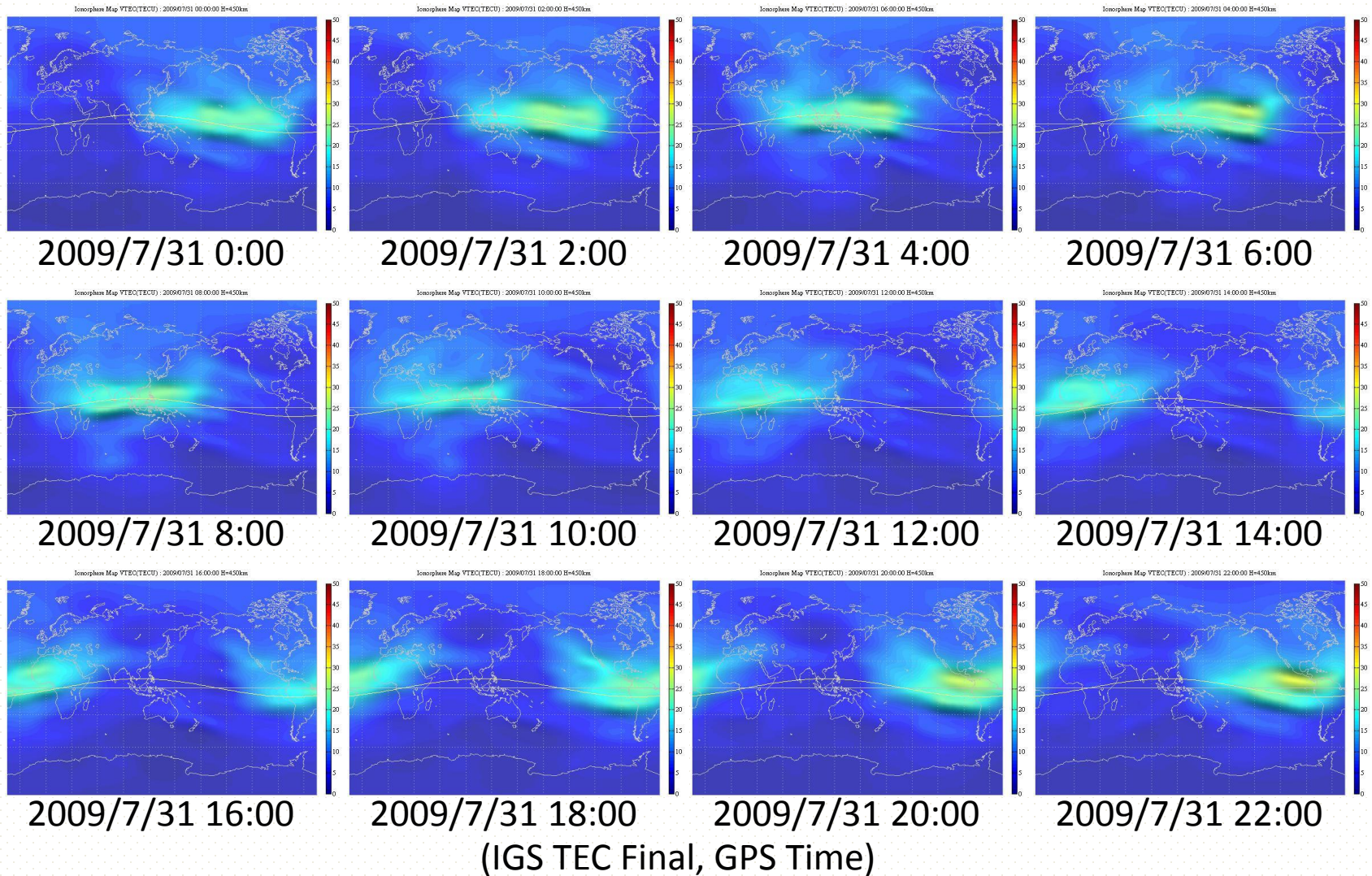
$$z' = \arcsin \frac{R_e \sin z}{R_e + H_{ion}}, \alpha = z - z'$$

$$\phi_{pp} = \arcsin(\cos \alpha \sin \phi + \sin \alpha \cos \phi \cos Az)$$

$$\lambda_{pp} = \lambda + \arcsin \frac{\sin \alpha \sin Az}{\phi_{pp}}$$



Ionospheric TEC Grid



Tropospheric Delay

Tropospheric Delay Model:

$$T = m_h(El)ZHD + m_w(El)ZWD$$

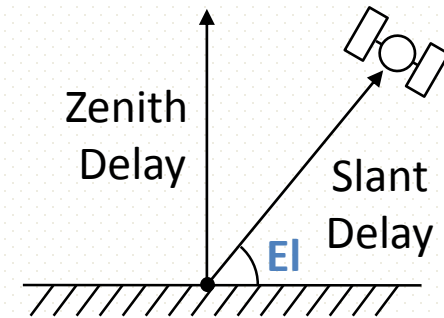
$$ZHD = \frac{0.0022768p}{1 - 0.00266\cos 2\phi - 2.8 \times 10^{-7} H}$$

: Zenith Hydrostatic Delay (m)

ZWD : Zenith Wet Delay (m)

$m_h(El)$: Hydrostatic Mapping Function

$m_w(El)$: Wet Mapping Function



ZWD to PWV (Precipitable Water Vapor):

$$T_m = 70.2 + 0.72T$$

$$PWV = \frac{1 \times 10^5}{R_v \left(k_2 - k_1 \frac{m_v}{m_d} + \frac{k_3}{T_m} \right)} ZWD$$

$$R_v = 461, k_1 = 77.6,$$

$$k_2 = 71.98, k_3 = 3.754 \times 10^5$$

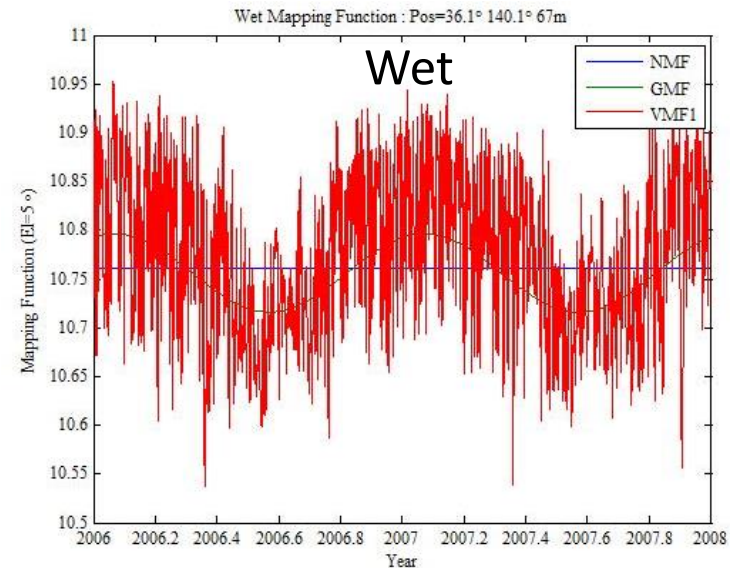
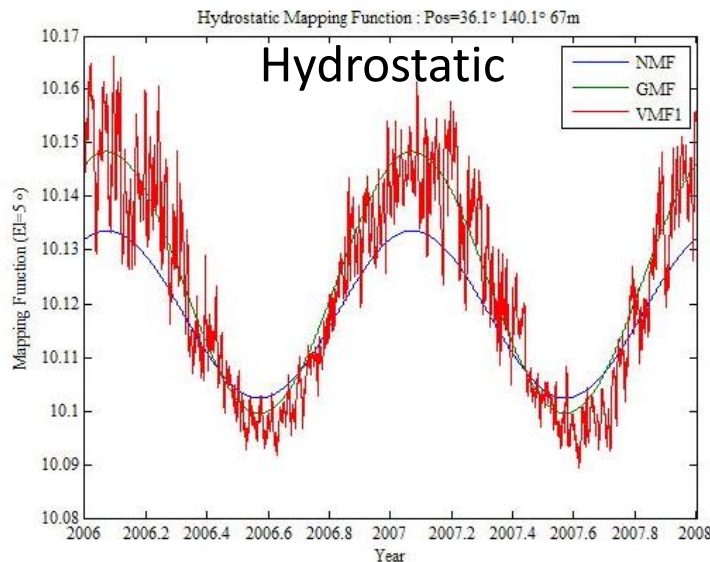
$$m_v = 18.0152, m_d = 28.9644$$

Mapping Function

$$m(El) = \frac{1 + \frac{a}{1 + \frac{b}{1 + c}}}{\sin(El) + \frac{a}{\sin(El) + \frac{b}{\sin(El) + c}}}$$

a, b, c : Mapping Function Coefficients

NMF, GMF, VMF1



(2006/1/1-2007/12/31, TSKB, El=5deg)

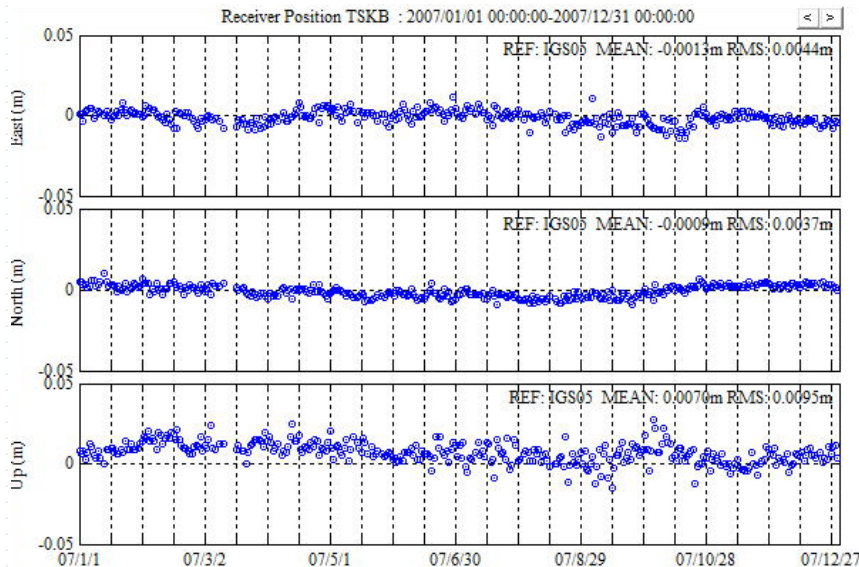
Tropospheric Gradient

Mapping Function with Horizontal Gradient:

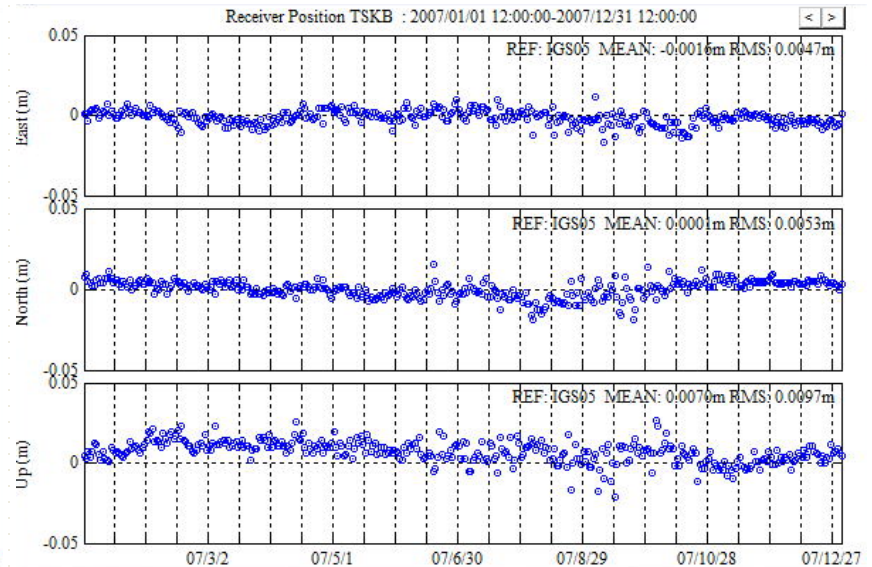
$$m(El, Az) = m_0(El) + m_0(El) \cot(El) (G_N \cos(Az) + G_E \sin(Az))$$

G_N, G_E : North/East Gradient Parameters

PPP Solutions with Gradient Estimation



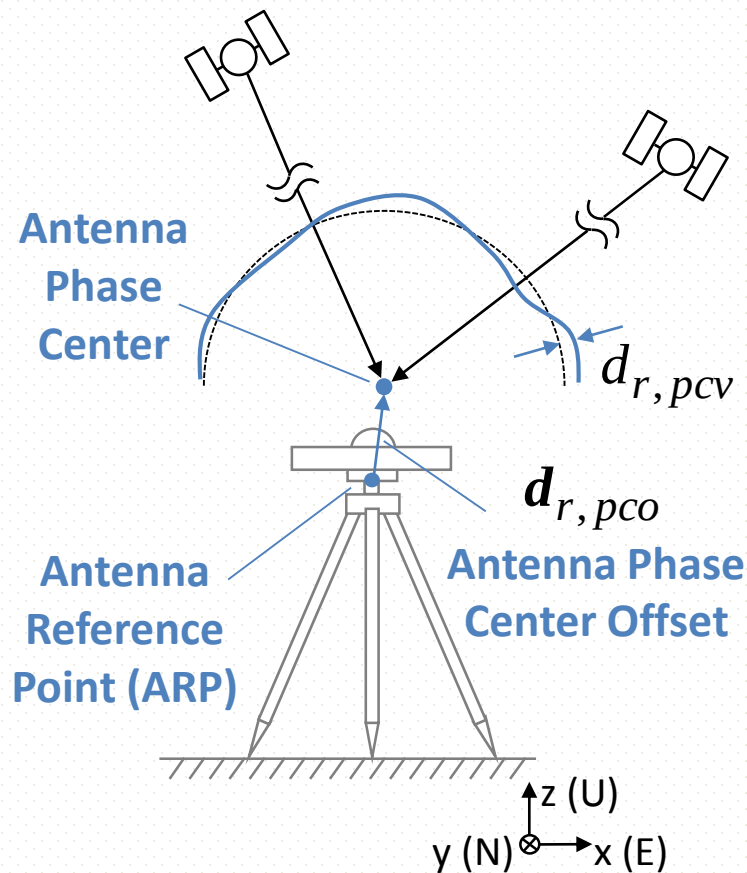
PPP Solutions without Gradient Estimation



2007/1/1-12/31, 24H-Static PPP, TSKB

Antenna Phase Center 1

Receiver Antenna Phase Center:



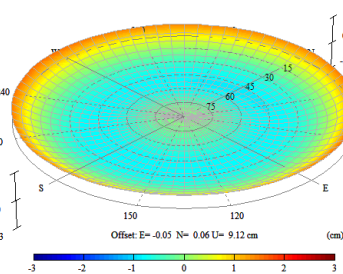
Antenna Phase Center Variation (PCV)

Choke-Ring Type



Antenna Phase Center Offset Variation : AOADM_T (L1)

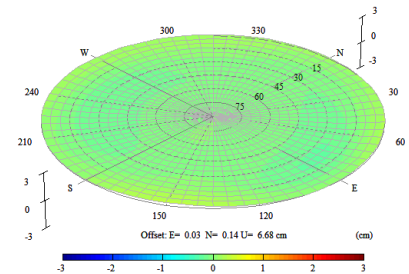
L1



Zero-Offset Type

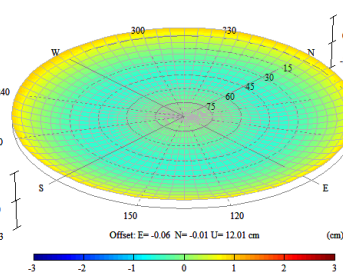


Antenna Phase Center Offset Variation : NOV702GG (L1)

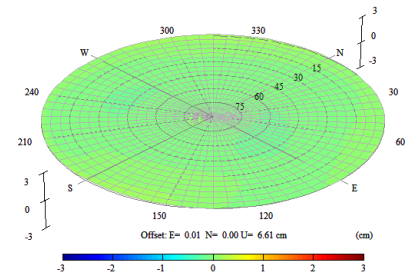


L2

Antenna Phase Center Offset Variation : AOADM_T (L2)



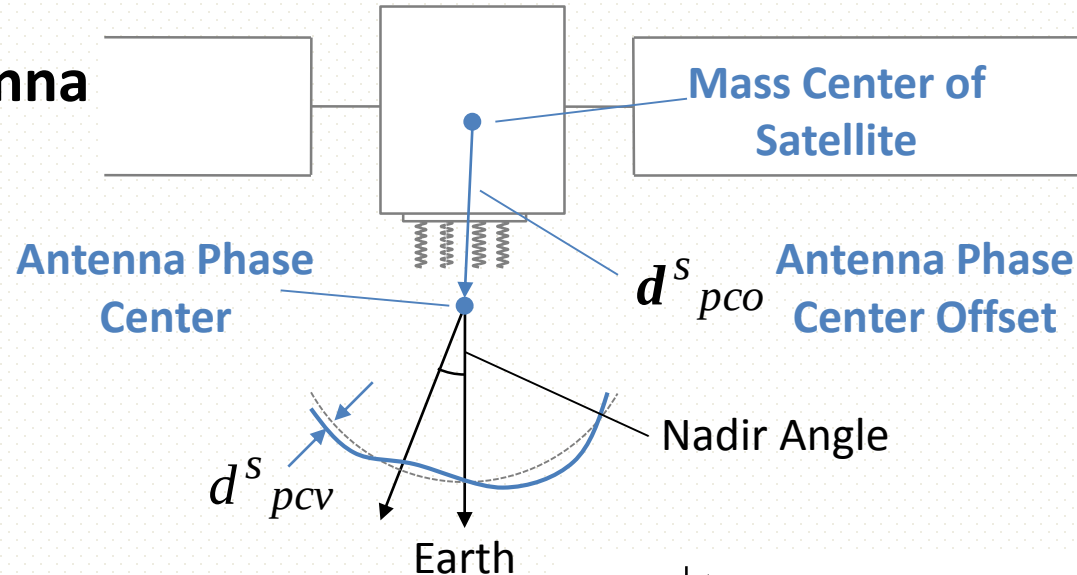
Antenna Phase Center Offset Variation : NOV702GG (L2)



IGS Absolute Antenna Model (IGS05.PCV)

Antenna Phase Center 2

Satellite Antenna Phase Center:

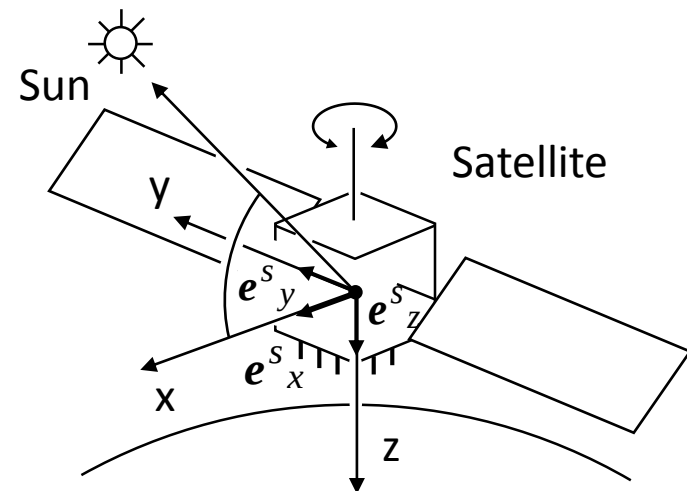


Satellite Coordinate to ECEF:

$$\mathbf{E}_{sat \rightarrow ecef} = (\mathbf{e}_x^s, \mathbf{e}_y^s, \mathbf{e}_z^s)$$

$$\mathbf{e}_z^s = -\frac{\mathbf{r}^s}{\|\mathbf{r}^s\|}, \mathbf{e}_s = \frac{\mathbf{r}_{sun} - \mathbf{r}^s}{\|\mathbf{r}_{sun} - \mathbf{r}^s\|}$$

$$\mathbf{e}_y^s = \frac{\mathbf{e}_z^s \times \mathbf{e}_s}{\|\mathbf{e}_z^s \times \mathbf{e}_s\|}, \mathbf{e}_x^s = \mathbf{e}_y^s \times \mathbf{e}_z^s$$

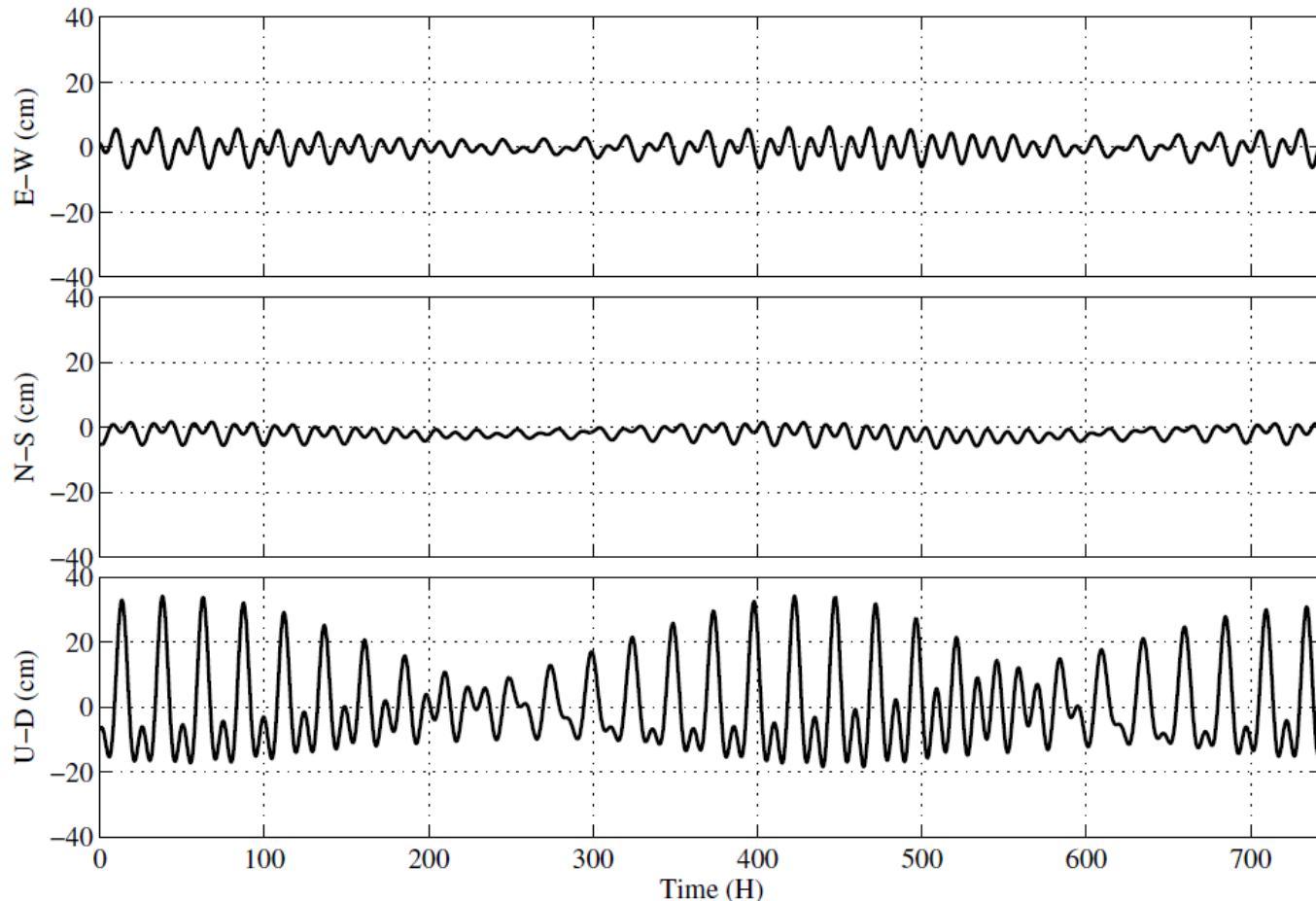


Site Displacement

- **Displacement of Ground-Fixed Receiver**
 - Solid Earth Tide
 - Ocean Tide Loading (OTL)
 - Pole Tide
 - Atmospheric Loading
- **Tide Model**
 - IERS Conventions 1996/2003/2010
 - Ocean Loading: Schwiderski, GOT99.2/00.2, CSR 3.0/4.0, FES99/2004, NAO99.b
 - $M_2, S_2, N_2, K_2, K_1, O_1, P_1, Q_1, M_1, M_m, S_{sa}$

Earth Tides

Earth Tides Model



IERS Conventions 1996 + NAO99.b, 2007/1/1-1/31, TSKB

Phase Wind-up Effect

- Relative rotation between satellite and receiver antennas effect to the measured phase of RHCP signal.

$$d_{pw} = \lambda \left\{ \text{sign}(\mathbf{e}_r^S \cdot (\mathbf{D}^S \times \mathbf{D}_r)) \arccos \frac{\mathbf{D}^S \cdot \mathbf{D}_r}{\|\mathbf{D}^S\| \|\mathbf{D}_r\|} / 2\pi + N \right\}$$

$\mathbf{D}^S = \mathbf{e}_x^S - \mathbf{e}_u^S (\mathbf{e}_u^S \cdot \mathbf{e}_x^S) - \mathbf{e}_u^S \times \mathbf{e}_y^S$: Dipole Vector of Satellite Antenna

$\mathbf{D}_r = \mathbf{e}_{r,x} - \mathbf{e}_r^S (\mathbf{e}_r^S \cdot \mathbf{e}_{r,x}) + \mathbf{e}_r^S \times \mathbf{e}_{r,y}$: Dipole Vector of Receiver Antenna

$\mathbf{E}_{ecef \rightarrow enu} = (\mathbf{e}_{r,x}^T, \mathbf{e}_{r,y}^T, \mathbf{e}_{r,z}^T)^T$: ECEF to ENU Transformation Matrix

$\mathbf{e}_r^S$: LOS Vector from Receiver to Satellite Antenna

N : Integer Ambiguity

Relativistic Effects

- **Satellite/Receiver:**
 - Frequency Shift by Earth Gravity (General Rel.)
 - Frequency Shift by Sun/Moon Gravity (General Rel.)
 - Second-Order Doppler-Shift by Motion (Special Rel.)
- **Signal Propagation:**
 - Sagnac Correction (Rotating Coordinates)
 - Shapiro Time Delay Effect
 - Lense-Thirring Drag

Satellite Clock Bias/Rate Correction
+ Periodic Term:

$$d_{rel} = -\frac{2\mathbf{r}^s \cdot \mathbf{v}^s}{c^2}$$

DD (Double Difference)

$$\Phi_{ub}^{ij} \equiv \lambda((\phi_u^i - \phi_b^i) - (\phi_u^j - \phi_b^j))$$

$$= \rho_{ub}^{ij} + c(dt_{ub}^{ij} - dT_{ub}^{ij}) - I_{ub}^{ij} + T_{ub}^{ij} + \lambda B_{ub}^{ij} + d_{ub}^{ij} + \varepsilon_\phi$$

$$= \rho_{ub}^{ij} - I_{ub}^{ij} + T_{ub}^{ij} + \lambda N_{ub}^{ij} + d_{ub}^{ij} + \varepsilon_\phi$$

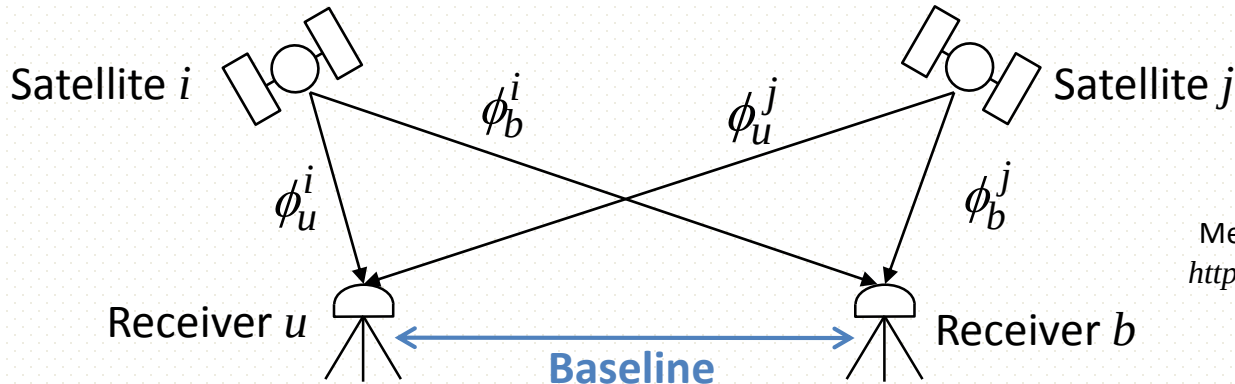
$$dt_{ub}^{ij} = dt_u^{ij} - dt_b^{ij} = 0, dT_{ub}^{ij} = dT_{ub}^i - dT_{ub}^j \approx 0$$

$$B_{ub}^{ij} = (\phi_{u,0} - \phi_0^i + N_u^i) - (\phi_{b,0} - \phi_0^i + N_b^i) - (\phi_{u,0} - \phi_0^j + N_u^j) + (\phi_{b,0} - \phi_0^j + N_b^j) = N_{ub}^{ij}$$

(short Baseline and same antenna type)

$$\Phi_{ub}^{ij} \approx \rho_{ub}^{ij} + \lambda N_{ub}^{ij} + \varepsilon_\phi$$

$$I_{ub}^{ij} = I_{ub}^i - I_{ub}^j \approx 0, T_{ub}^{ij} = T_{ub}^i - T_{ub}^j \approx 0, d_{ub}^{ij} = d_{ub}^i - d_{ub}^j \approx 0$$



Memo for Misra & Enge:
<http://gpspp.sakura.ne.jp/diary200608.htm>

Baseline Processing

Nonlinear-LSE:

Parameter Vector:

$$\mathbf{x} = (\mathbf{r}_u^T, N_{ub}^{s_2s_1}, N_{ub}^{s_3s_1}, \dots, N_{ub}^{s_ms_1})^T$$

Measurement Vector:

$$\mathbf{y} = (\mathbf{y}_{t_1}^T, \mathbf{y}_{t_2}^T, \dots, \mathbf{y}_{t_n}^T)^T$$

Meas Model, Design Matrix:

$$\mathbf{h}(\mathbf{x}) = (\mathbf{h}_{t_1}(\mathbf{x})^T, \mathbf{h}_{t_2}(\mathbf{x})^T, \dots, \mathbf{h}_{t_n}(\mathbf{x})^T)^T$$

$$\mathbf{H} = (\mathbf{H}_{t_1}^T, \mathbf{H}_{t_2}^T, \dots, \mathbf{H}_{t_n}^T)^T$$

Meas Error Covariance:

$$\mathbf{R} = \text{blkdiag}(\mathbf{R}_{t_1}, \mathbf{R}_{t_2}, \dots, \mathbf{R}_{t_n})$$

Solution (Static/Float):

$$\hat{\mathbf{x}} = \mathbf{x}_0 + (\mathbf{H}^T \mathbf{R}^{-1} \mathbf{H})^{-1} \mathbf{H}^T \mathbf{R}^{-1} (\mathbf{y} - \mathbf{h}(\mathbf{x}_0))$$

$$\mathbf{y}_{t_k} = (\Phi_{ub,t_k}^{s_2s_1}, \Phi_{ub,t_k}^{s_3s_1}, \dots, \Phi_{ub,t_k}^{s_ms_1})^T$$

$$\mathbf{h}_{t_k}(\mathbf{x}) = \begin{pmatrix} \rho_{u,t_k}^{s_2s_1} - \rho_{b,t_k}^{s_2s_1} + \lambda N_{ub}^{s_2s_1} \\ \rho_{u,t_k}^{s_3s_1} - \rho_{b,t_k}^{s_3s_1} + \lambda N_{ub}^{s_3s_1} \\ \vdots \\ \rho_{u,t_k}^{s_ms_1} - \rho_{b,t_k}^{s_ms_1} + \lambda N_{ub}^{s_ms_1} \end{pmatrix}$$

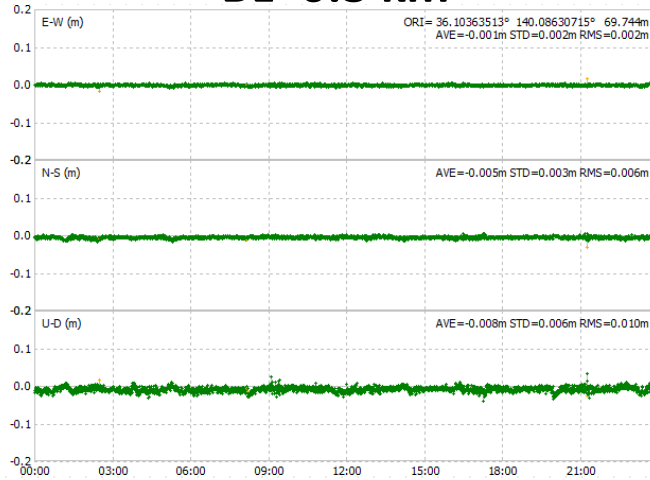
$$\mathbf{H}_{t_k} = \begin{pmatrix} -\mathbf{e}_{u,t_k}^{s_2s_1 T} & \lambda & 0 & \dots & 0 \\ -\mathbf{e}_{u,t_k}^{s_3s_1 T} & 0 & \lambda & \dots & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ -\mathbf{e}_{u,t_k}^{s_ms_1 T} & 0 & 0 & \dots & \lambda \end{pmatrix}$$

$$\mathbf{R}_{t_k} = \begin{pmatrix} 4\sigma_\phi^2 & 2\sigma_\phi^2 & \dots & 2\sigma_\phi^2 \\ 2\sigma_\phi^2 & 4\sigma_\phi^2 & \dots & 2\sigma_\phi^2 \\ \vdots & \vdots & \ddots & \vdots \\ 2\sigma_\phi^2 & 2\sigma_\phi^2 & \dots & 4\sigma_\phi^2 \end{pmatrix}$$

$\mathbf{r}_b$: Fixed Base-Station Position

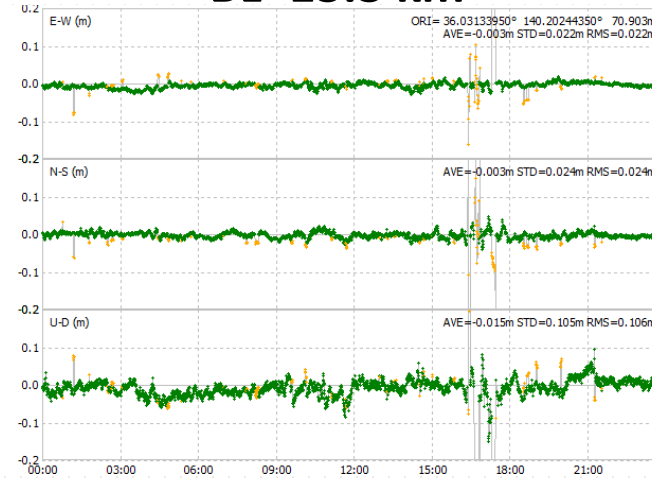
Effect of Baseline Length

BL=0.3 km



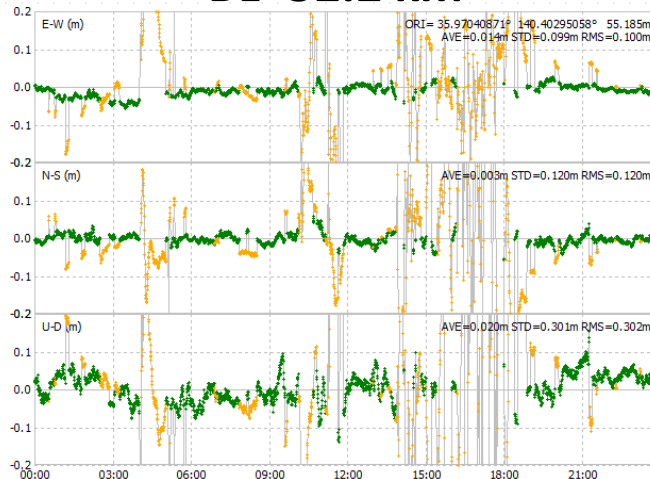
RMS Error:
E: 0.2cm
N: 0.6cm
U: 1.0cm
Fix Ratio:
99.9%

BL=13.3 km



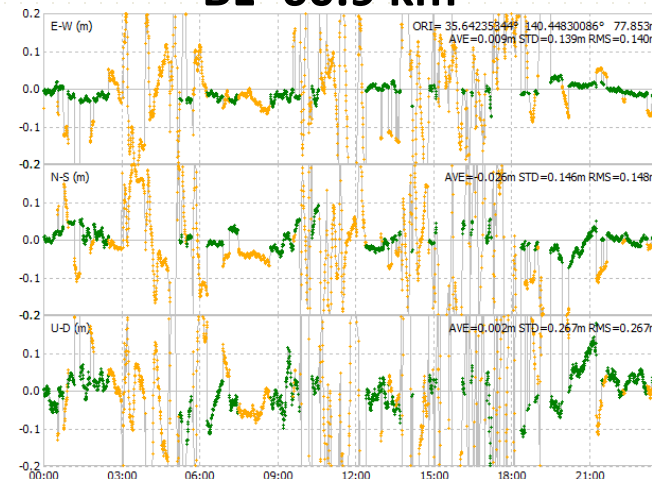
RMS Error:
E: 2.2cm
N: 2.4cm
U: 10.6cm
Fix Ratio:
94.2%

BL=32.2 km



RMS Error:
E: 10.0cm
N: 12.0cm
U: 30.2cm
Fix Ratio:
64.3%

BL=60.9 km



RMS Error:
E: 14.0cm
N: 14.8cm
U: 26.7cm
Fix Ratio:
44.4%

(24 hr Kinematic ●: Fixed Solution ●: Float Solution)

Integer Ambiguity Resolution

- **Objectives**
 - More accurate than float solutions
 - Fast converge of solutions
- **Many AR Strategies**
 - Simple Integer rounding
 - Multi-frequency wide-lane and narrow-lane generation
 - Search in coordinate domain
 - Search in ambiguity domain
 - AFM, FARA, LSAST, LAMBDA, ARCE, HB-L³, Modified Cholesy Decomposition, Null Space, FAST, OMEGA, ...

ILS (Integer Least Square Estimation)

Problem:

$$\begin{aligned} \mathbf{x} &= (\mathbf{a}^T, \mathbf{b}^T)^T, \mathbf{H} = (\mathbf{A}, \mathbf{B}) \\ \mathbf{y} &= \mathbf{H}\mathbf{x} + \mathbf{v} = \mathbf{A}\mathbf{a} + \mathbf{B}\mathbf{b} + \mathbf{v} \\ \tilde{\mathbf{x}} &= \arg \min_{\mathbf{a} \in \mathbf{Z}^n, \mathbf{b} \in \mathbf{R}^m} (\mathbf{y} - \mathbf{H}\mathbf{x})^T \mathbf{Q}_y^{-1} (\mathbf{y} - \mathbf{H}\mathbf{x}) \end{aligned}$$

Strategy:

(1) Conventional LSE

$$\hat{\mathbf{x}} = \begin{pmatrix} \hat{\mathbf{a}} \\ \hat{\mathbf{b}} \end{pmatrix} = \mathbf{Q}_x \mathbf{H}^T \mathbf{Q}_y^{-1} \mathbf{y}, \mathbf{Q}_x = \begin{pmatrix} \mathbf{Q}_a & \mathbf{Q}_{ab} \\ \mathbf{Q}_{ba} & \mathbf{Q}_b \end{pmatrix} = (\mathbf{H}^T \mathbf{Q}_y \mathbf{H})^{-1}$$

(2) **Search Integer Vector** with Minimum Squared Residuals

$$\tilde{\mathbf{a}} = \arg \min_{\mathbf{a} \in \mathbf{Z}^n} (\hat{\mathbf{a}} - \mathbf{a})^T \mathbf{Q}_a^{-1} (\hat{\mathbf{a}} - \mathbf{a})$$

(3) Improve solution

$$\tilde{\mathbf{b}} = \hat{\mathbf{b}} - \mathbf{Q}_{ba} \mathbf{Q}_a^{-1} (\hat{\mathbf{a}} - \tilde{\mathbf{a}})$$

LAMBDA

Teunissen, P.J.G. (1995)

The least-squares ambiguity decorrelation adjustment: a method for fast GPS integer ambiguity estimation. *Journal of Geodesy*, Vol. 70, No. 1-2, pp. 65-82.

- **ILS Estimation with:**

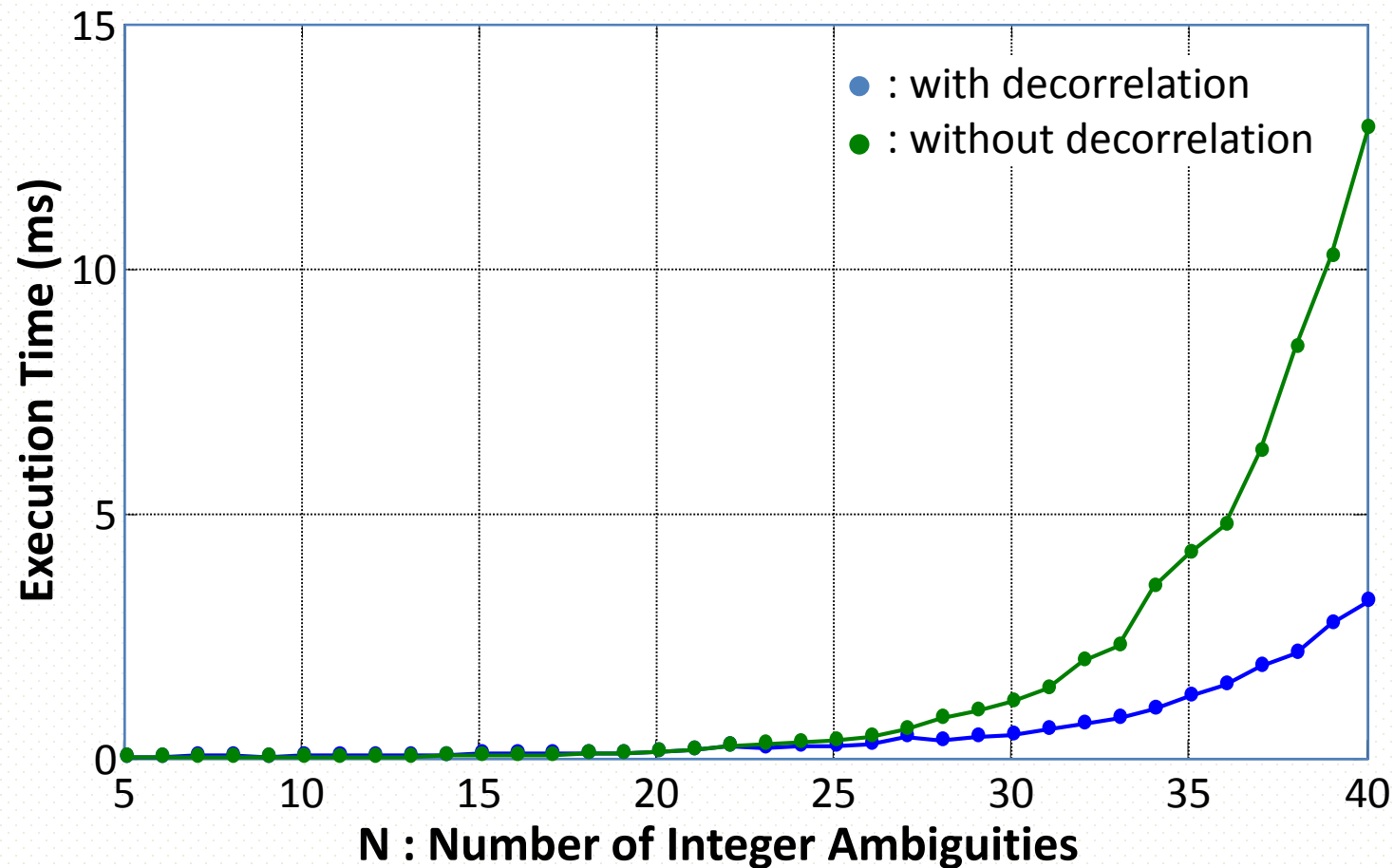
- Shrink Integer Search Space with "Decorrelation"
- Efficient Tree Search Strategy
- Similar to *Closest Point Search with LLL Lattice Basis Reduction* Algorithm

$$\check{\mathbf{a}} = \arg \min_{\mathbf{a} \in \mathbf{Z}^n} (\hat{\mathbf{a}} - \mathbf{a})^T \mathbf{Q}_a^{-1} (\hat{\mathbf{a}} - \mathbf{a})$$



$$\begin{aligned} \hat{\mathbf{z}} &= \mathbf{Z}^T \hat{\mathbf{a}}, \mathbf{Q}_z = \mathbf{Z}^T \mathbf{Q}_a \mathbf{Z} \\ \check{\mathbf{z}} &= \arg \min_{\mathbf{z} \in \mathbf{Z}^n} (\hat{\mathbf{z}} - \mathbf{z})^T \mathbf{Q}_z^{-1} (\hat{\mathbf{z}} - \mathbf{z}) \\ \check{\mathbf{a}} &= \mathbf{Z}^{-T} \check{\mathbf{z}} \end{aligned}$$

Performance of LAMBDA



(Pentium 4 3.2GHz, Intel C/C++ 8.0)

RTK (Real-Time Kinematic)

- **Technique with Baseline Processing**
 - Real-time Position of Rover Antenna
 - Transmit Reference Station Data to Rover via Comm. Link
 - OTF (On-the-Fly) Integer Ambiguity Resolution
 - Typical Accuracy: $1 \text{ cm} + 1 \text{ ppm} \times \text{BL RMS (Horizontal)}$
 - Applications:
Land Survey, Construction Machine Control, Precision Agriculture etc.



RTK Application



Geodetic Survey



Construction
Machine Control



Precision Agriculture



ITS (Intelligent
Transport System)



Mobile Mapping
System



Sports

Network RTK (NRTK)

- **Extension of RTK**

- RTK without User Reference Station
- Sparse Networked Reference Stations
- Correction Messages via Mobile-Phone Network
- Format: **VRS**, **FKP**, MAC, RTCM 2.3, RTCM 3.1
- Server S/W: Trimble GPSNet, GEO++ GNSMART, ...
- NTRIP Networked Transport of RTCM via Internet Protocol

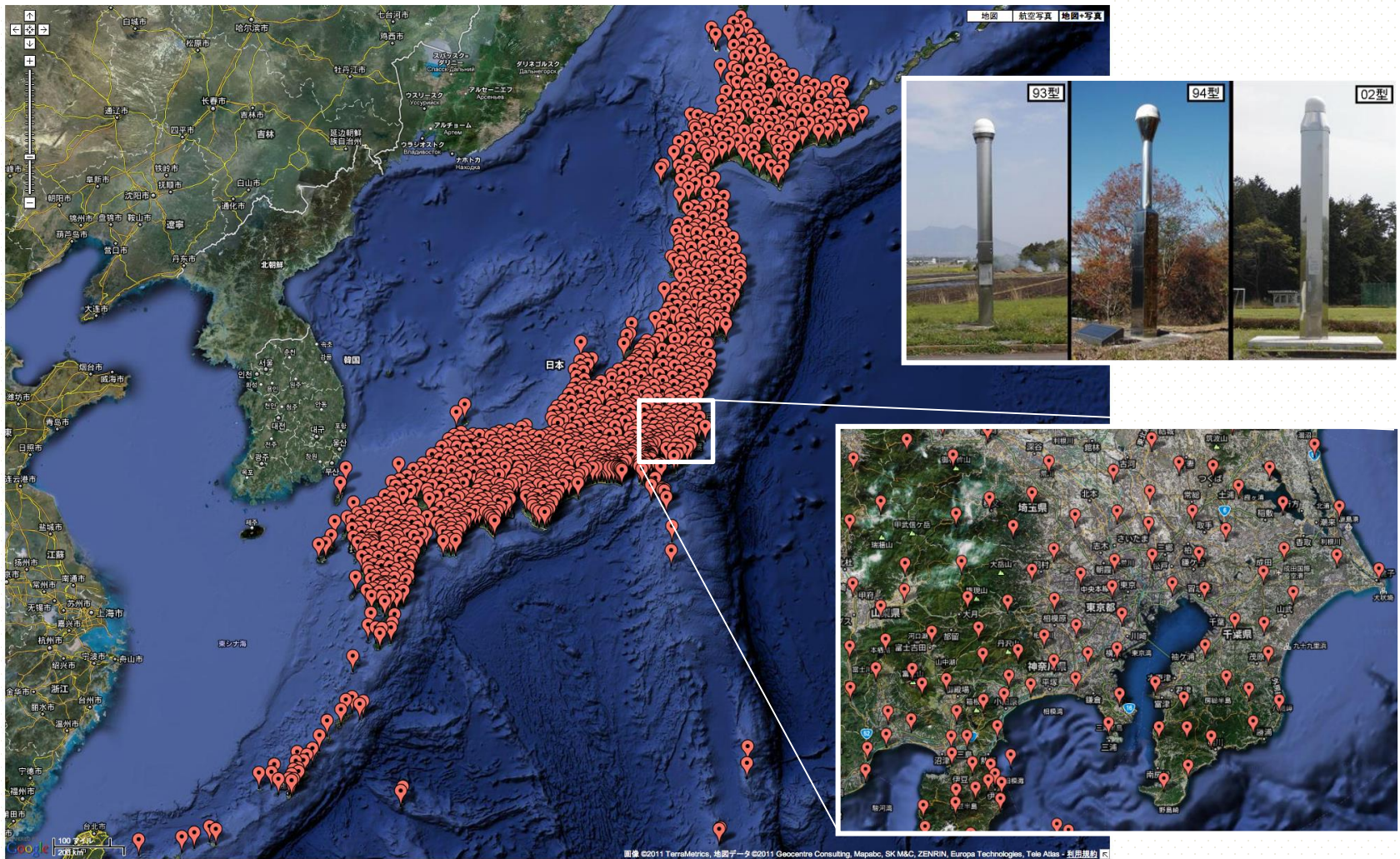
- **NRTK Service in Japan**

- GEONET: ~1200 Reference Stations by GSI
- NGDS (www.gpsdata.co.jp), JENOBAs (www.jenoba.jp)

Japanese GEONET

GEONET STATIONS MAP by Google Map : [GEONET Stations](#)

[IGS Map](#) | [Home](#)



The station coordinates are based on the ITRF2000 positions on 2007/1/1 provided by GSI. Height: ellipsoidal height (WGS84).

(<http://terras.gsi.go.jp/ja/index.htm>)

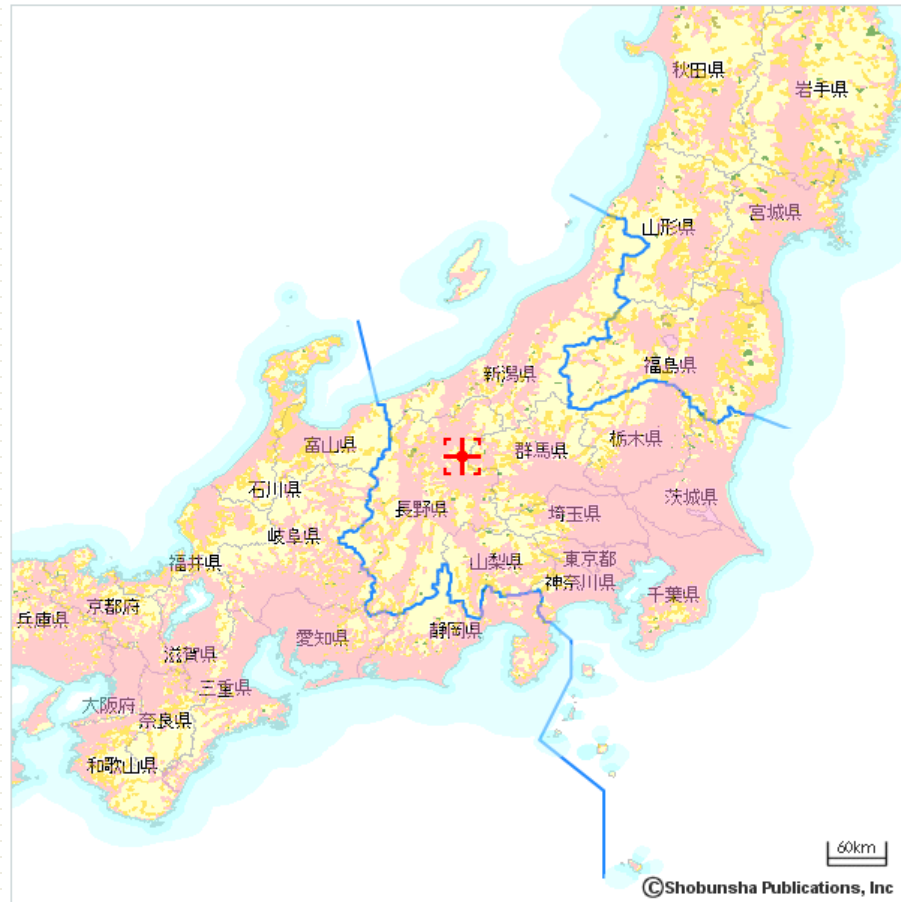
Considerations for RTK System

- **Rover**
 - Single vs. Dual-freq, Update Rate, GNSS, Receiver-cost
 - CPU Power for external processing
 - INS-integration for obstacles
- **Reference Station**
 - Baseline-Length vs. Performance
 - Self-provided vs. NRTK Service
 - Coverage, Receiver-cost, Operational-cost, Service-fee
- **Communication Link**
 - Coverage, Band-width, Latency, Link-cost

Communication Link for RTK

- **Local (<300 m)**
 - Serial, USB, LAN, ... (wired)
 - Radio Modem, WiFi, ZigBee, DSRC, ... (wireless)
- **Regional (<1,000 km)**
 - Analog-phone, ISDN, Dedicated Link, ... (wired)
 - Mobile-phone (Analog, 2G, 3G, ...), ... (wireless)
- **Global (<10,000 km)**
 - Internet
 - GEO Satellite Link (Inmarsat, WideStar II, ...)
 - LEO Satellite Link (Iridium, Orbicom, ...)

Coverage by Mobile-phone N/W



NTT docomo FOMA (2008/9)

(<http://servicearea.nttdocomo.co.jp>)

B-5

RTKLIB Practice (3)

RTK by Playback Data

- **Objective**

RTK of by Playback Data

- **Program**

rtklib_2.4.2p9¥bin¥rtknavi.exe

- **Data**

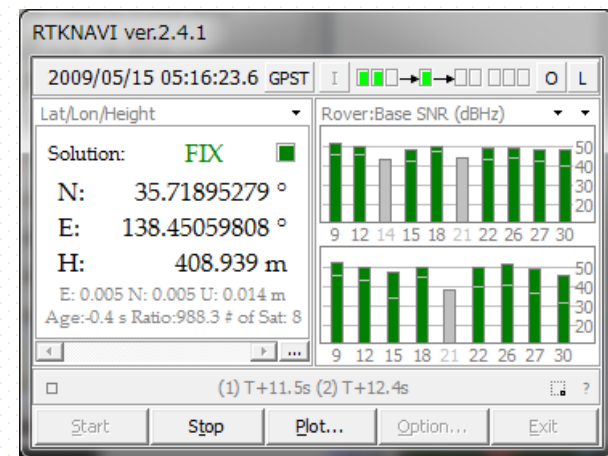
sample2¥

oemv_2009515c.gps (NovAtel)

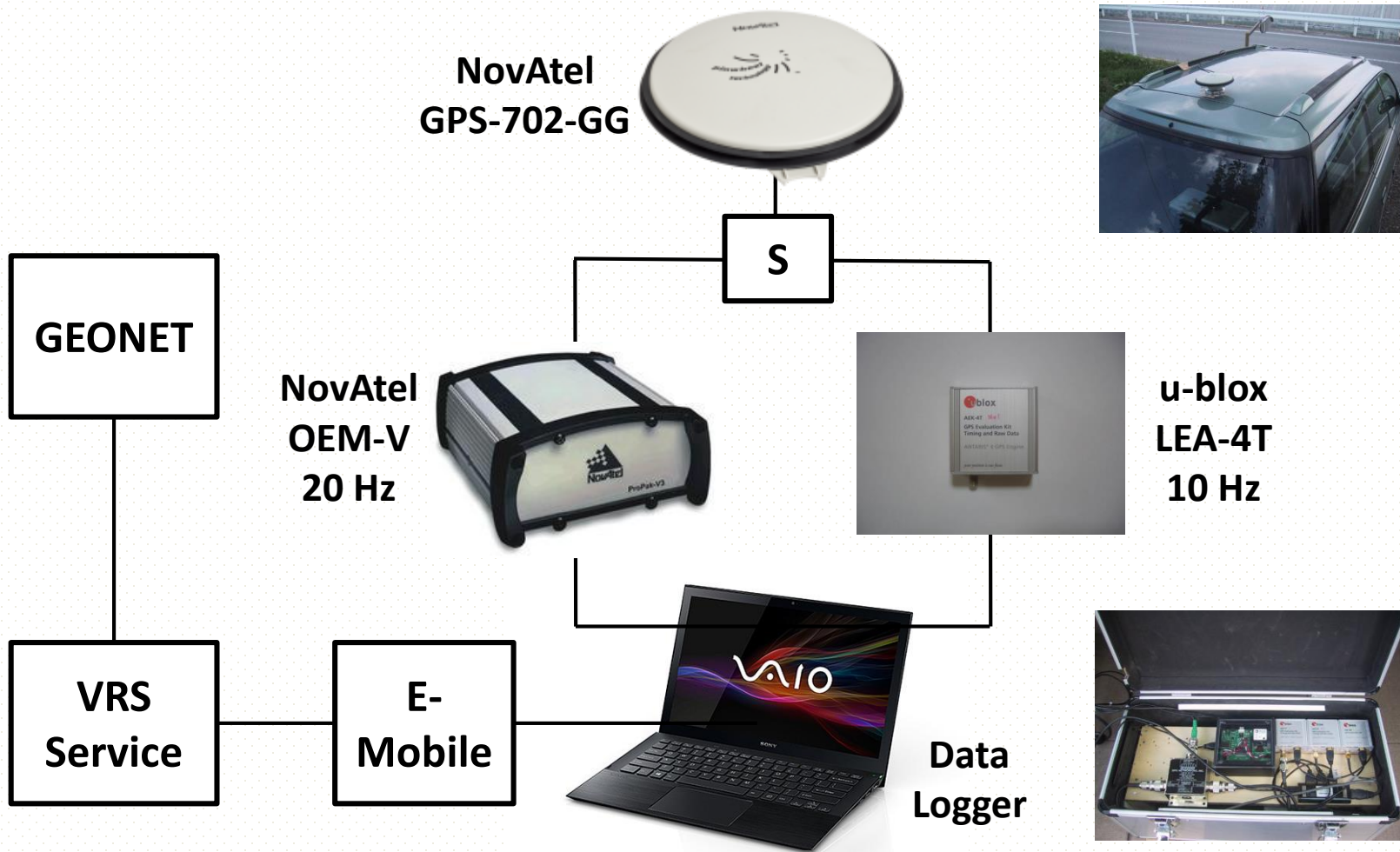
ubx_20090515c.ubx (u-blox)

0263_20090515c.rtc3 (VRS)

RTKNAVI

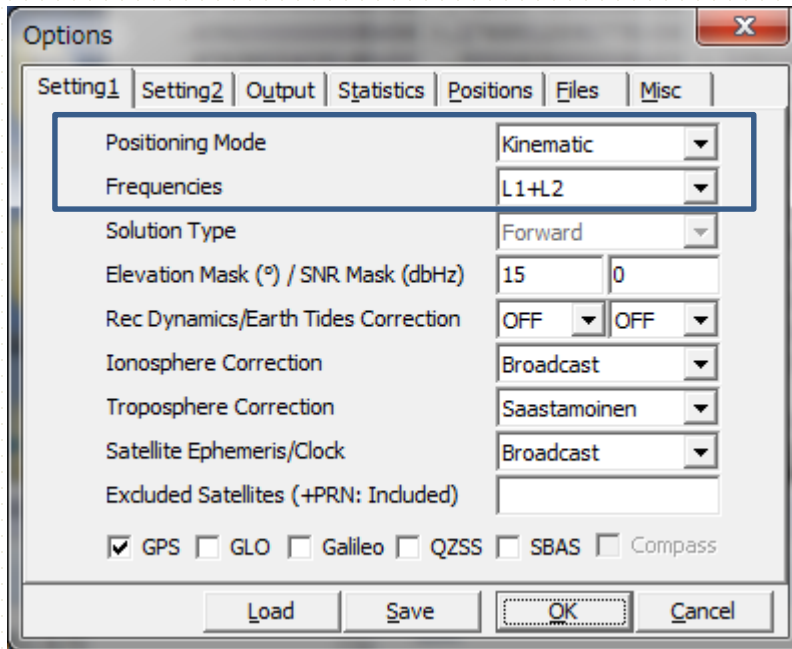


Playback Data



RTKNAVI - Options

Setting1

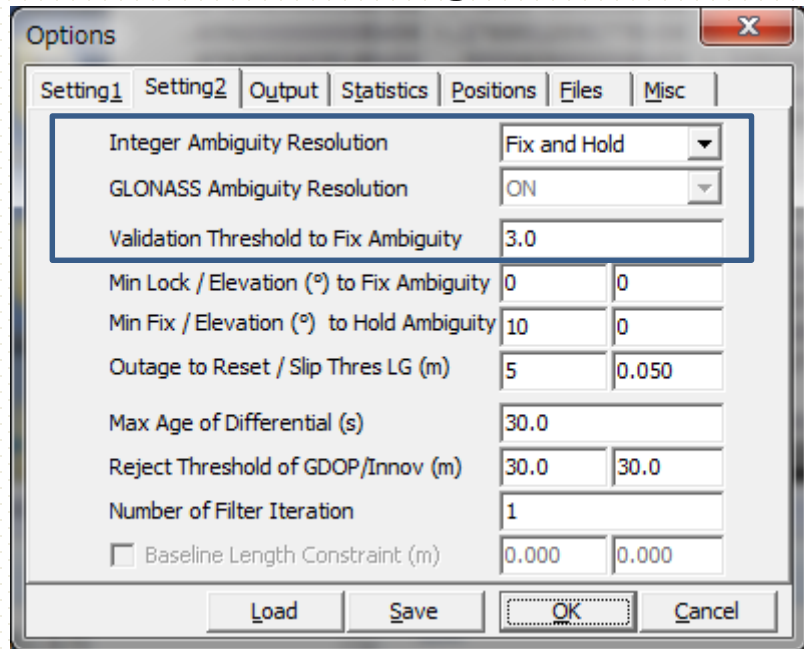


The 'Setting1' tab of the RTKNAVI Options dialog box contains the following settings:

Setting	Value
Positioning Mode	Kinematic
Frequencies	L1+L2
Solution Type	Forward
Elevation Mask (°) / SNR Mask (dBHz)	15 / 0
Rec Dynamics/Earth Tides Correction	OFF / OFF
Ionosphere Correction	Broadcast
Troposphere Correction	Saastamoinen
Satellite Ephemeris/Clock	Broadcast
Excluded Satellites (+PRN: Included)	
GPS	☒
GLO	☐
Galileo	☐
QZSS	☐
SBAS	☐
Compass	☐

Buttons: Load, Save, OK, Cancel

Setting2



The 'Setting2' tab of the RTKNAVI Options dialog box contains the following settings:

Setting	Value
Integer Ambiguity Resolution	Fix and Hold
GLONASS Ambiguity Resolution	ON
Validation Threshold to Fix Ambiguity	3.0
Min Lock / Elevation (°) to Fix Ambiguity	0 / 0
Min Fix / Elevation (°) to Hold Ambiguity	10 / 0
Outage to Reset / Slip Thres LG (m)	5 / 0.050
Max Age of Differential (s)	30.0
Reject Threshold of GDOP/Innov (m)	30.0 / 30.0
Number of Filter Iteration	1
Baseline Length Constraint (m)	☐ 0.000 / 0.000

Buttons: Load, Save, OK, Cancel

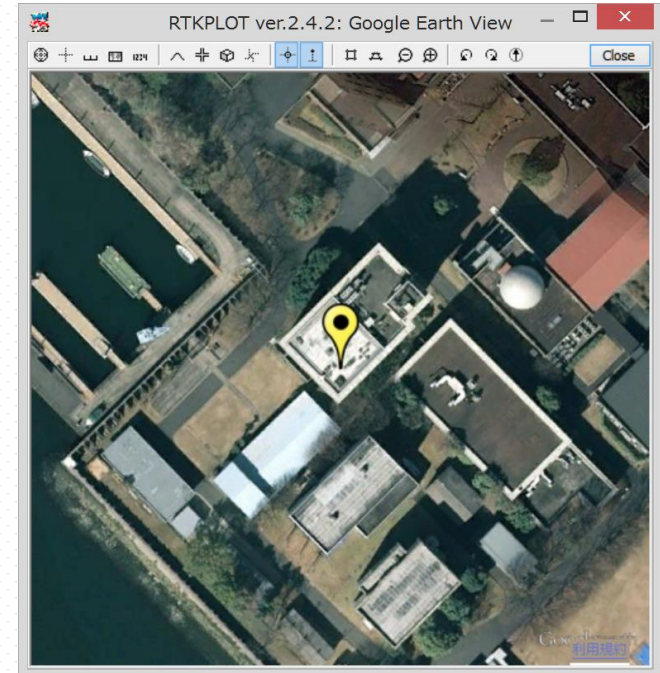
Reference Station for RTK

Receiver:
Trimble NetR9



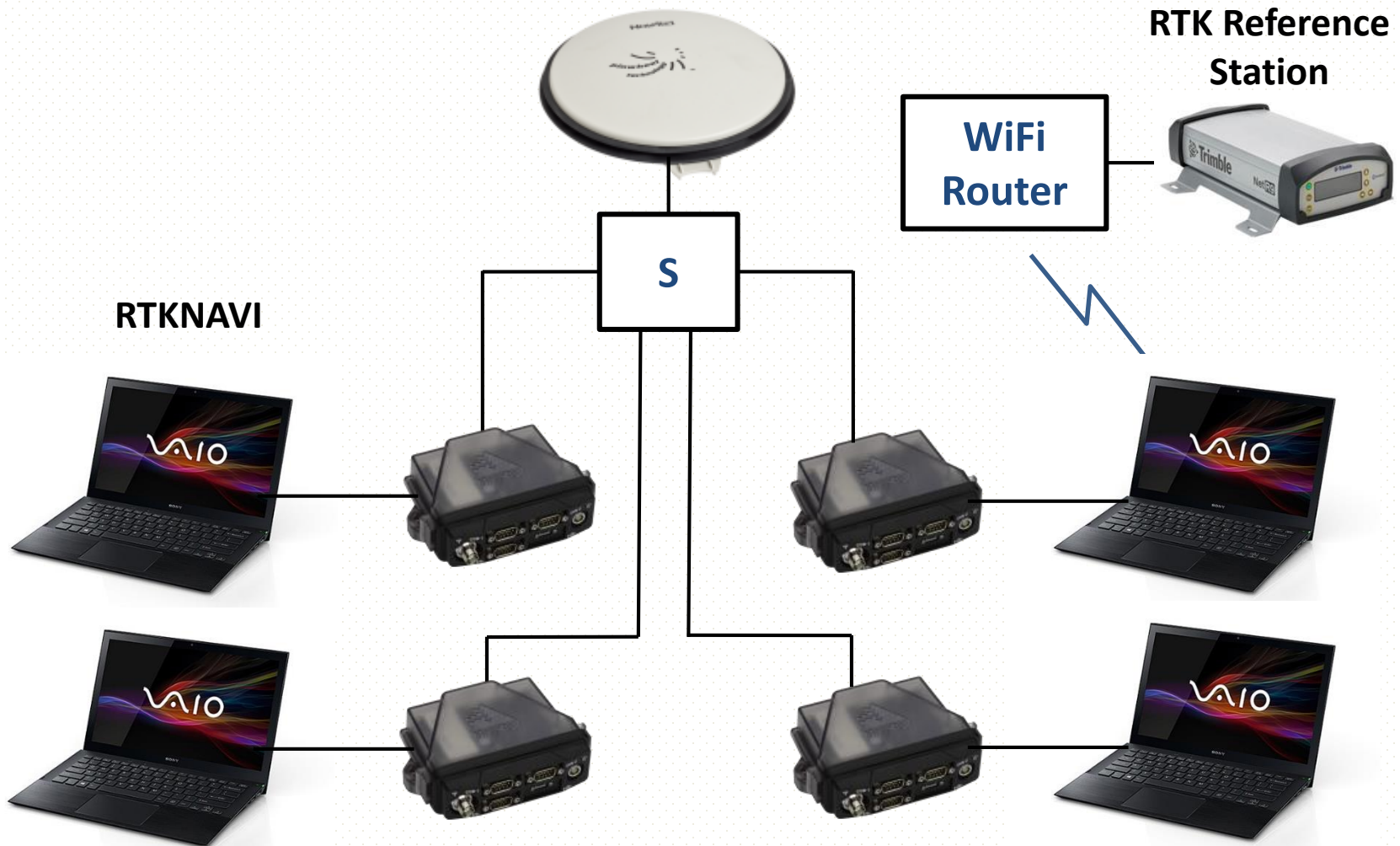
IP-Addr : *.***.***.*****
Port : 2101
MountP : RTCM3
USER-ID : *****
PW : ****
Data : RTCM 3, GPS+GLO

IP-Addr : *.***.***.*****
Port : 2102
MountP : BINEX
USER-ID : *****
PW : ****
Data : BINEX, GPS+GLO+GAL+QZS+BDS



Lat: 35.666243069
Lon: 139.792308111
Height: 59.8700

RTK Setup for Port Cruise



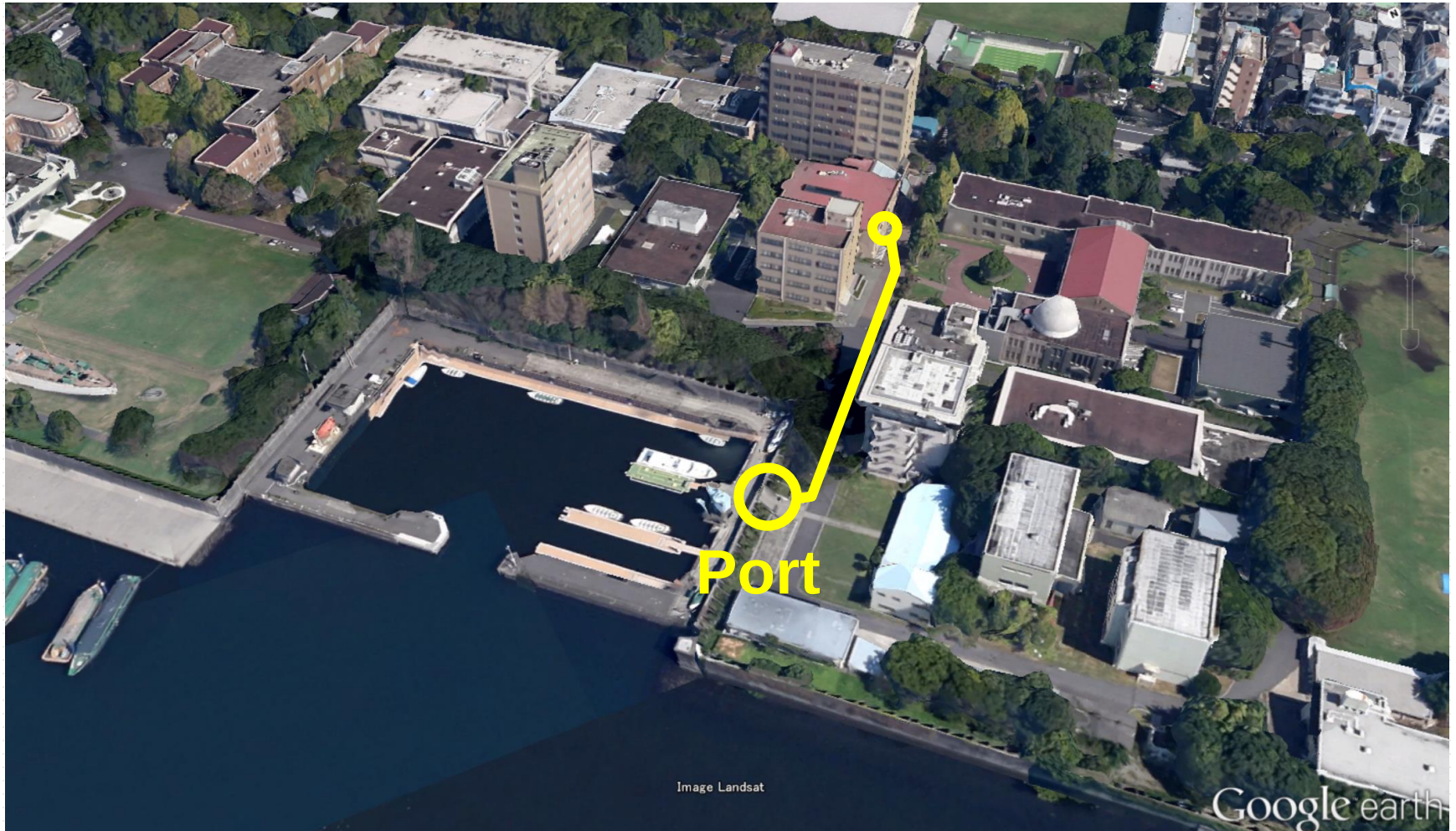
What is AIS ? by JRC

Port Cruise Demo & RTKLIB Practice (4)

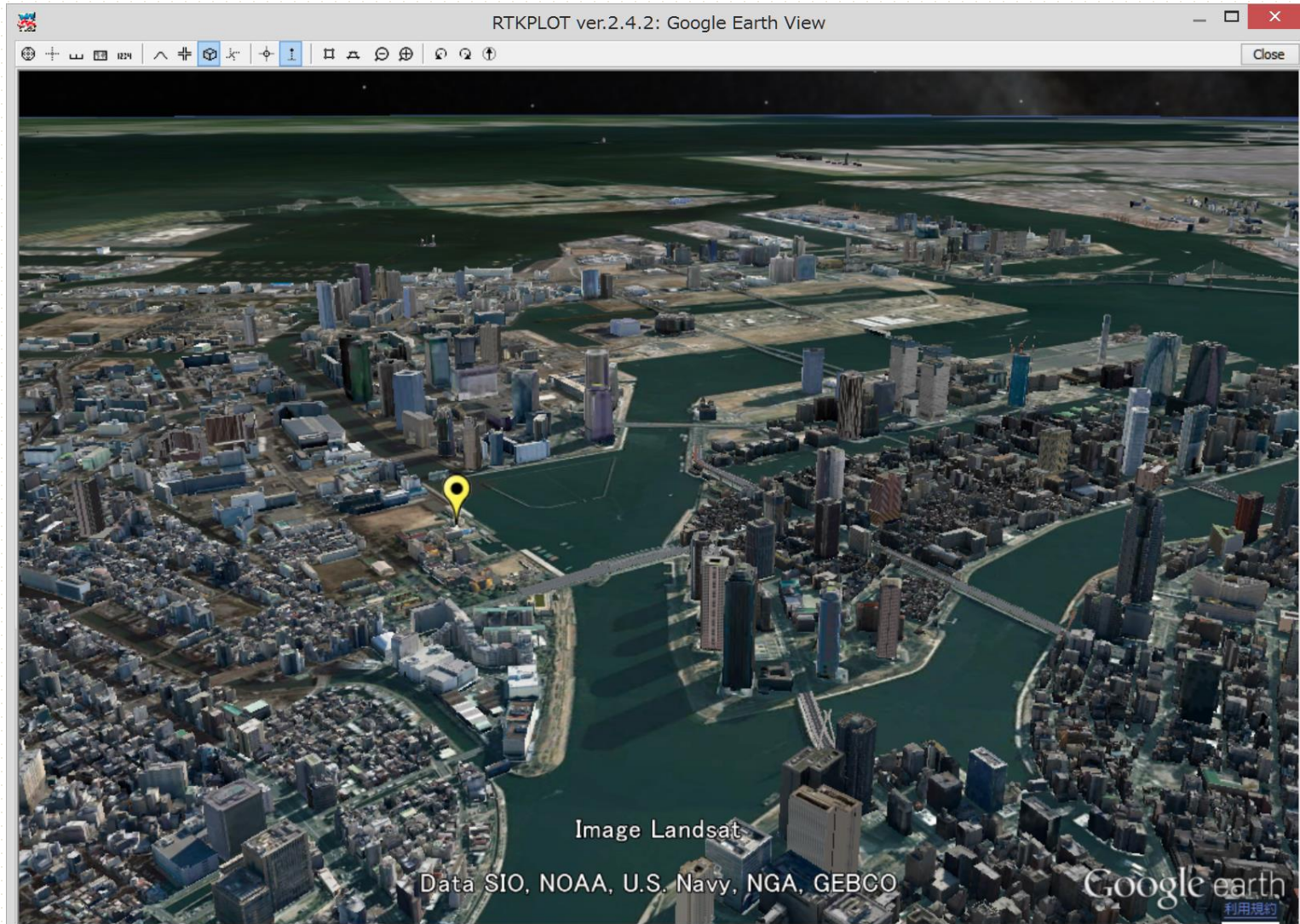
Port Cruise Schedule

- **Group 1 (A, B, C, D)**
 - **Loading** : **12:55 (keep it!)**
 - **Start** : **13:15**
 - **Return** : **14:20**
- **Group 2 (E, F, G, H)**
 - **Loading** : **14:15 (keep it!)**
 - **Start** : **14:35**
 - **Return** : **15:40**
- **Waiting Group**
 - Self Practice of RTKLIB on the Ground

Loading of Boat



Port Cruise with RTK



B-6

Advanced Topics

Advanced Topics

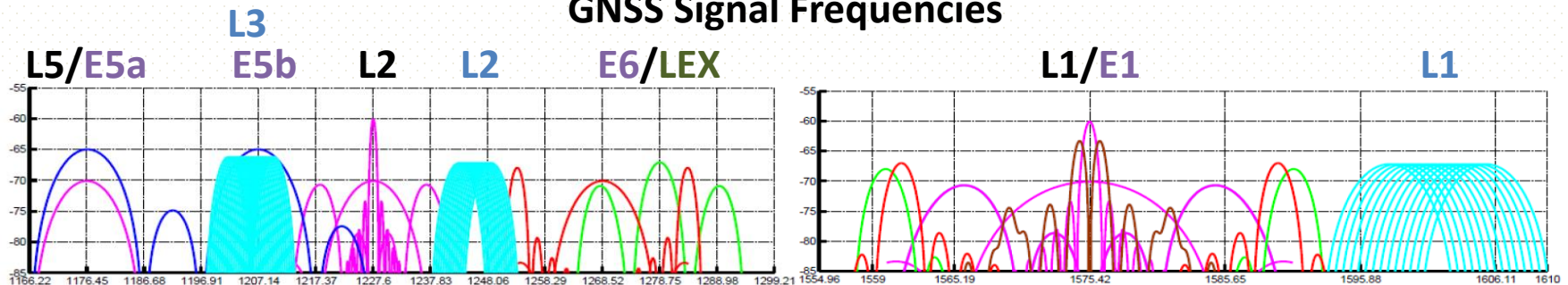
- **Multi-GNSS RTK**
- **Long-Baseline RTK**
- **INS-Aided RTK**
- **RTK-PPP**

GNSS Evolution

Number of Planned GNSS Satellites

System	2010	2013	2016	2019
GPS	31	31	32	32
GLONASS	23 (+2)	24 (+3)	24 (+3)	24 (+3)
Galileo	0	4	18	27 (+3)
Compass	6	16	30	32 (+3)
QZSS	1	1	4	7
IRNSS	0	7	7	7
SBAS	7	8	11	11
Total	68	91	126	140

GNSS Signal Frequencies



(Y.Yang, COMPASS: View on Compatibility and Interoperability, 2009)

Multi-GNSS RTK Performance

RTK Performance: Baseline 13.3 km, Instantaneous AR

		El Mask=15°				El Mask=30°			
GPS	Galileo	Fixing Ratio	RMS Error (cm)			Fixing Ratio	RMS Error (cm)		
			E-W	N-S	U-D		E-W	N-S	U-D
L1	-	49.7%	4.6	8.1	19.0	23.3%	71.4	115.0	289
GPS L1+L2	-	99.0%	1.4	1.3	1.9	87.6%	3.4	10.5	15.5
L1,L2,L5	-	99.0%	1.4	1.3	1.9	87.3%	3.4	10.5	15.6
L1	E1	98.8%	1.3	1.2	1.9	90.1%	1.2	2.1	2.7
GPS+GAL L1	E1	98.9%	1.4	1.2	1.7	98.7%	1.2	1.0	1.6
L1,L2	E1	98.9%	1.4	1.2	1.7	98.7%	1.2	1.0	1.6
L1,L2,L5	E1,E5a, E5b	98.9%	1.5	1.3	2.0	98.9%	1.3	1.1	1.8

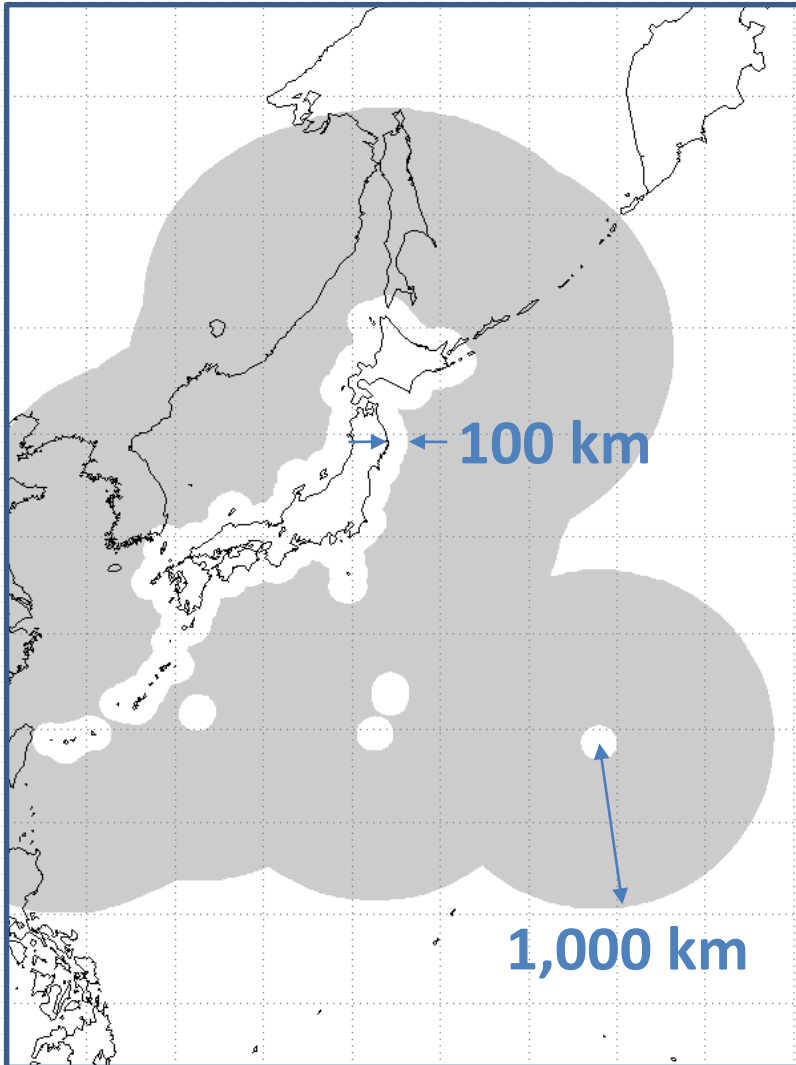
Multi-GNSS Receiver

- **Moore's Law**
 - More correlators
 - More tracking channels
 - More powerful embedded CPU
- **Consumer-grade Multi-GNSS Receiver**
 - SkyTraq: GPS + GLONASS
 - STMicro: GPS + GLONASS
 - Broadcom: GPS + GLONASS + QZSS
 - u-blox: GPS + Galileo

Issues for Multi-GNSS RTK

- **Multi-GNSS Integration Issue**
 - Time-system, Coordinate-system
 - Receiver H/W Biases
- **Multi-code System Issue**
 - L1C/A-L1P(Y)-L1Cd-L1Cp, L2P(Y)-L2C, L5I-L5Q
 - Quarter cycle phase-shift problem
- **GLONASS FDMA Issue**
 - Receiver Inter-channel biases (Receiver Interoperability)
 - Calibration Message Standard
 - Antenna Calibration

Long-Baseline RTK



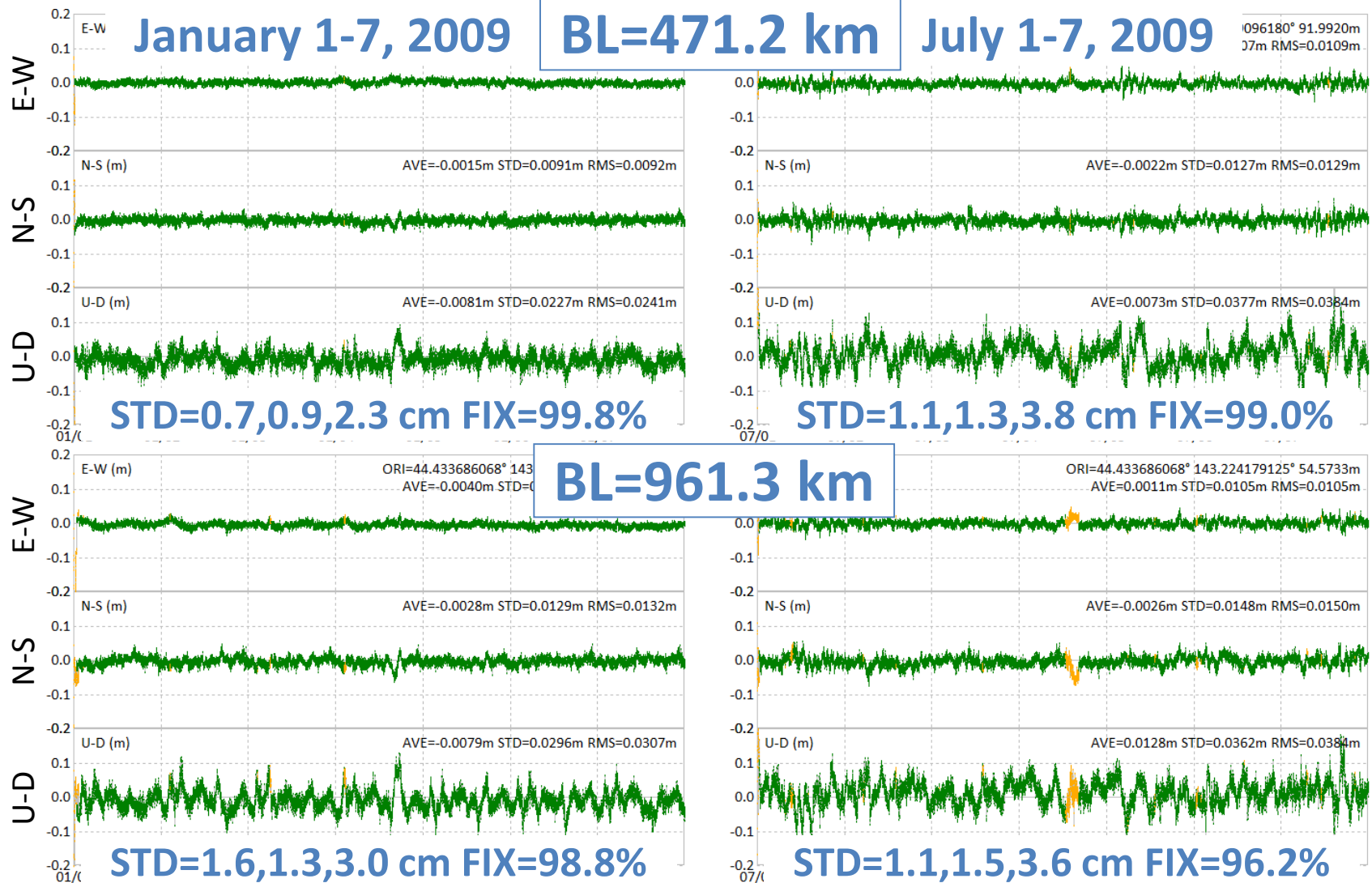
**GPS Tsunami
Monitoring System
(Currently ~15 km off-shore)**

<http://www.tsunamigps.com>

Long-Baseline RTK Strategy

	BL (km)	Error Elimination				Strategy
		Ephem	Ionos	Tropos	Others	
S	0 – 10	Broadcast	-	-	-	Conventional RTK
M	10 – 100	Broadcast	Dual-Freq	-	-	
			Interpolation		-	Network RTK
L	100 – 1,000	Real-time Precise (IGU)	Dual-Freq	Estimate ZTD + MF	Earth Tides	Long-Baseline RTK
VL	>1,000	Non-RT Precise (IGR, IGS)	Dual-Freq	Estimate ZTD + MF	Earth Tides, Ph-WU	Post- Processing or PPP

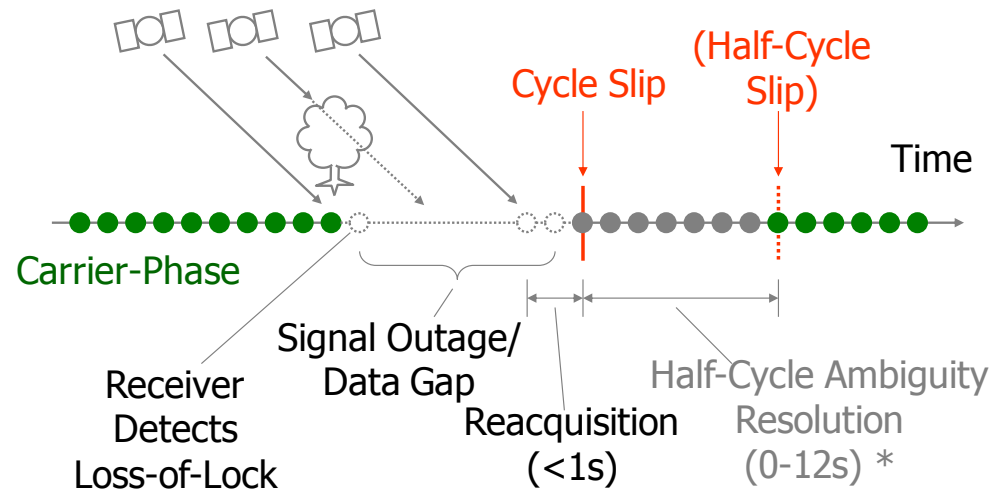
Long-Baseline RTK with RTKLIB



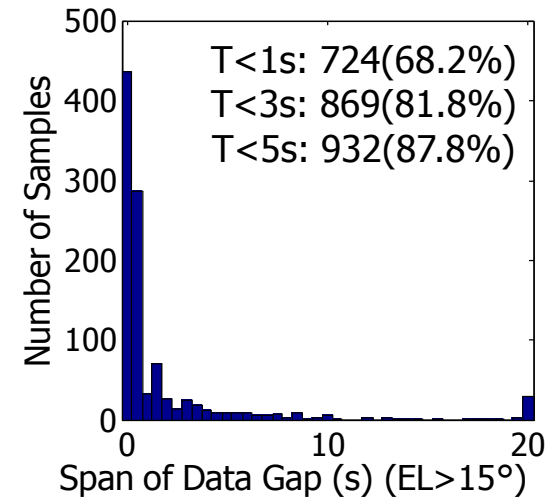
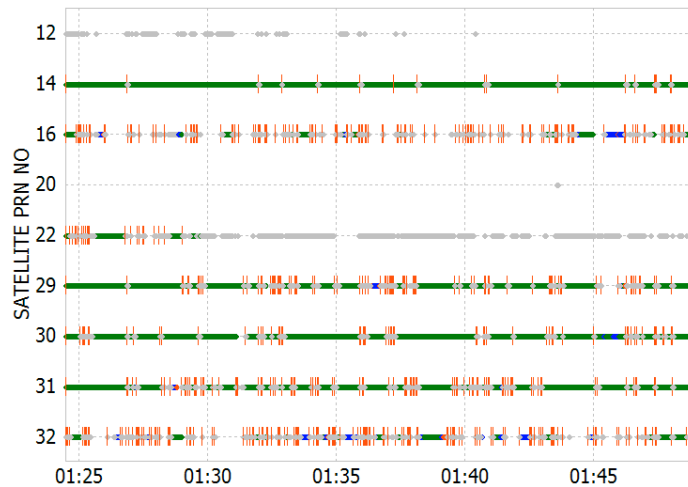
Mobile AP issues for RTK

- **Cycle-Slips**
 - Frequent cycle-slip with around obstacles
 - Miss-detection of cycle-slip
- **Low Solution Availability**
 - Long acquisition time by weak signal (Low C/N0)
 - Half-cycle ambiguity resolution with Costas-PLL
 - Low fixing ratio
- **High Noise Level**
 - High multipath level even in carrier-phase
 - Jamming by RFI

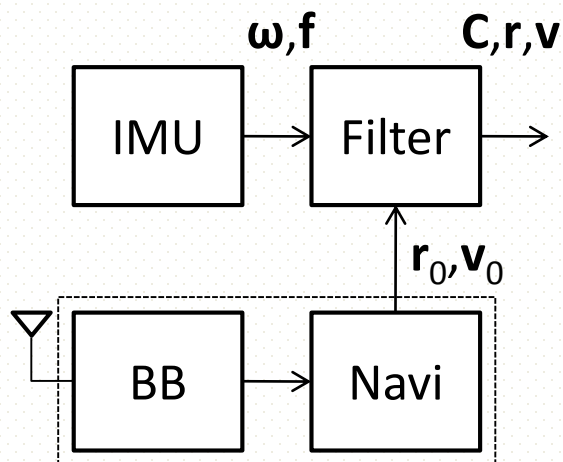
Cycle-Slips



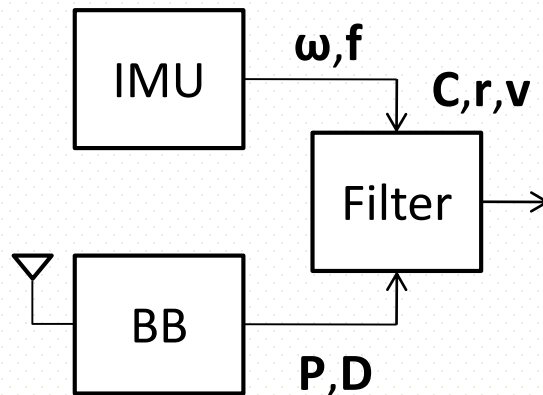
* Depend on Receiver



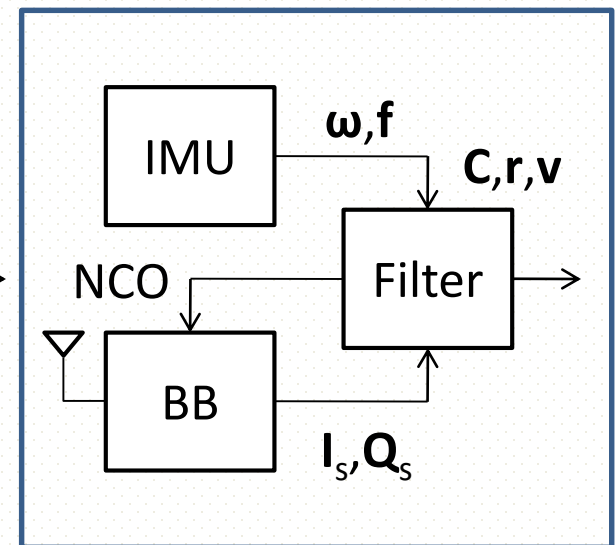
INS-Aided RTK



**Loosely-Coupled
Integration**



**Tightly-Coupled
Integration**



**Deep Integration
(Ultra-Tightly)**

High sensitivity
(DLL, PLL)
Slip resistance

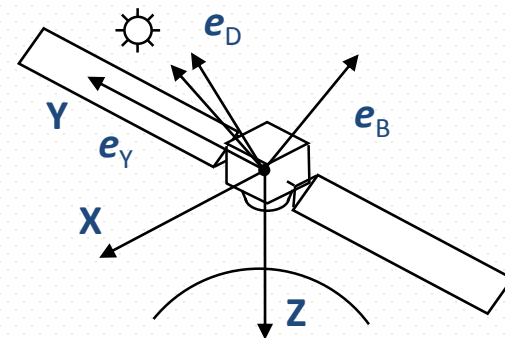
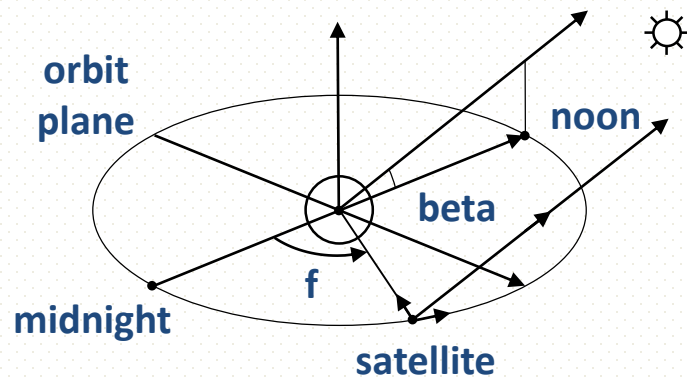
RTK-PPP

- **Combination of RTK and PPP**
 - Precise Orbits and Clocks
 - Ambiguity Resolution in PPP
 - Local Augmentation (Iono. and Tropos.)
- **RTCM SSR (RTCM 3.2, 3.5.12)**
 - Level 1: Precise Orbits, Clock and Code Biases
 - Level 2: Iono. (VTEC)
 - Level 3: Iono. (STEC), Tropos. and Phase Biases

Precise Orbits and Clock

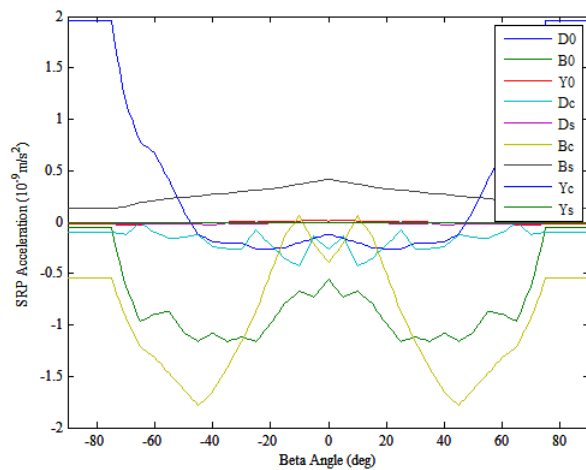
- **Satellite Orbit Models**
 - EGM 2008+solid earth tide+FES2004
 - Sun, Moon, Venus and Jupiter with JPL DE421
 - Empirical SRP model, ...
- **Measurement Models**
 - ZD Iono-free phase+ pseudorange, 2nd-order-iono
 - ZTD+gradient estimation with GPT+GMF/VMF1
 - IERS DEHANTIDEINEL+FES2004+pole tide+CMC
- **ECI-ECEF Coordinates Transformation**
 - IAU 2000A/2006 by IAU SOFA

SRP Model

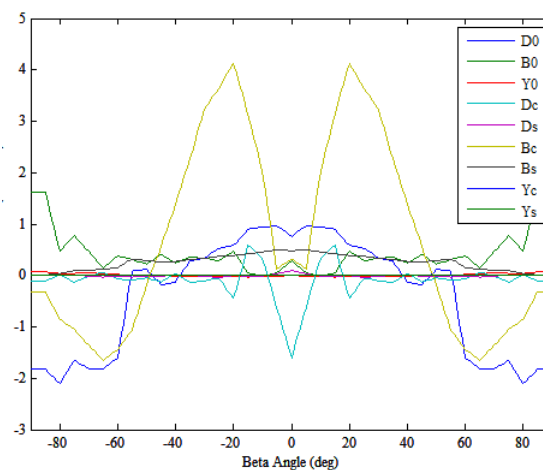


$$\mathbf{a}_{\text{srp}} = S \left((D_0 + D_C \cos f + D_S \sin f) \mathbf{e}_D + (B_0 + B_C \cos f + B_S \sin f) \mathbf{e}_B + (Y_0 + Y_C \cos f + Y_S \sin f) \mathbf{e}_Y \right) \times 10^{-9} \text{ (m/s}^2\text{)}$$

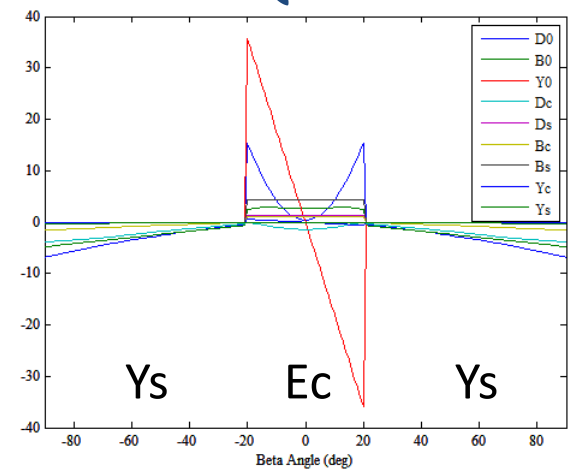
GPS Block IIR



GLONASS



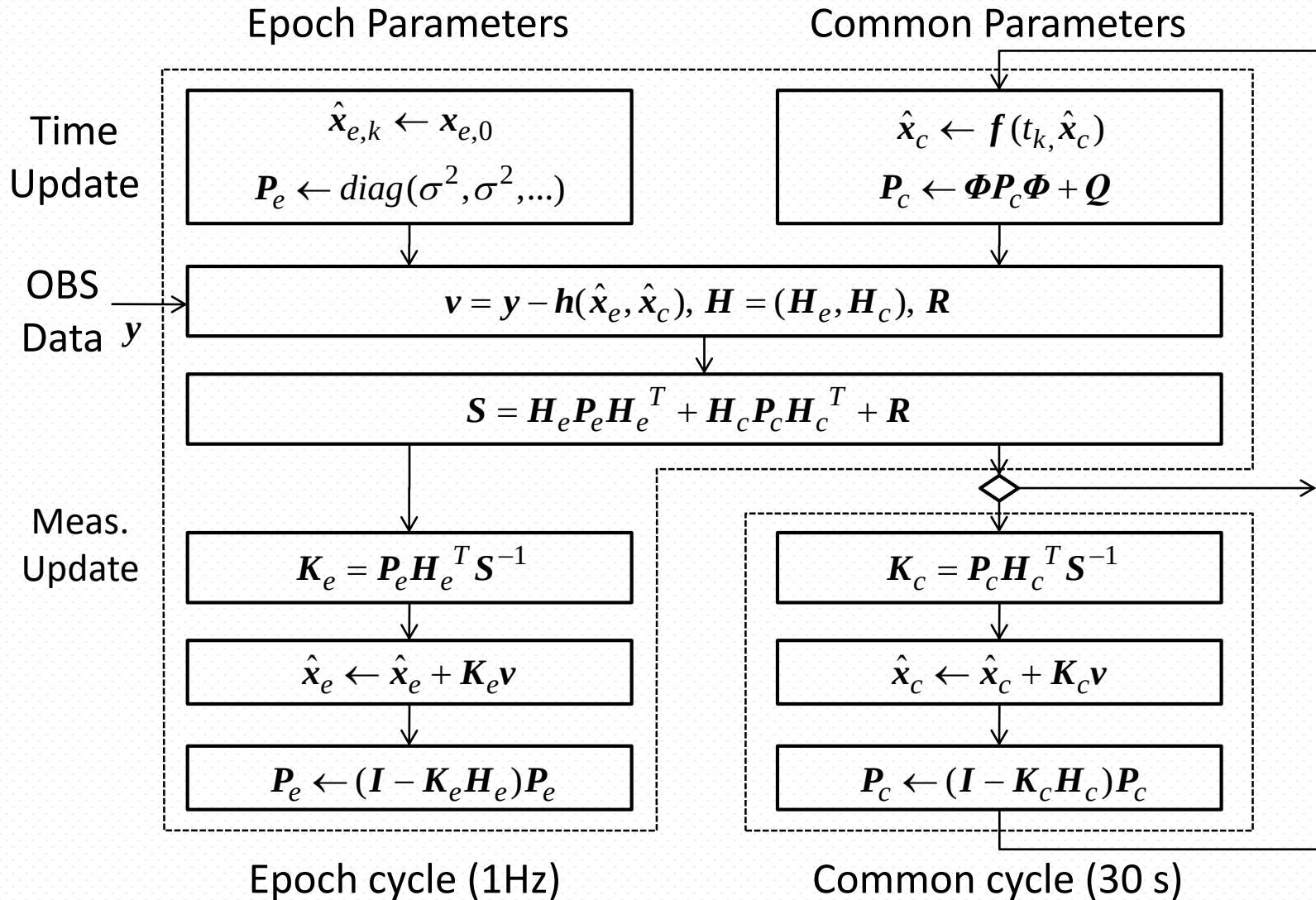
QZSS



Parameter Adjustment

	Offline	Real-Time
Algorithm	Iterated Weighted LSQ	Dual-Cycle-EKF
Estimated Parameters	Orbit, SRP/Emp-Acc, Clock, Position, ZTD/Grad, Ambiguity, Bias, EOP	
Measurements	ZD Carrier-Phase and Pseudo-range	
Numerical Solver	NEQ by Cholesky Factorization	Numerical Stable EKF
Clock Estimation	Parameter Elimination in NEQ	State as White-Noise or Random-Walk
Integer Ambiguity Resolution	Network AR (Ge., 2005)	Real-Time Network AR

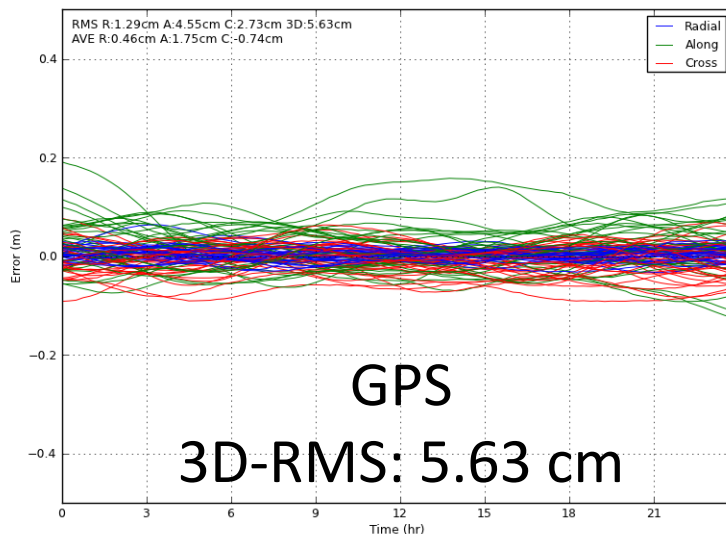
Dual-Cycle-EKF



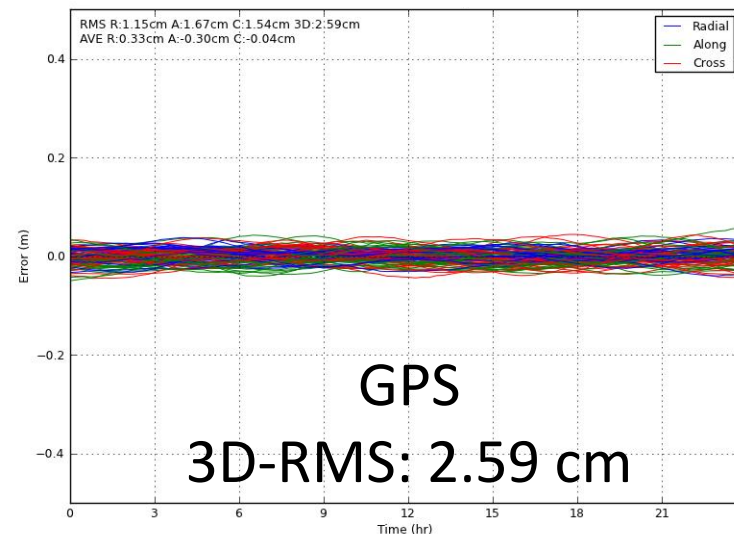
Network AR

- Dynamic baseline selection to convert ZD to DD
- WL and NL DD ambiguities by rounding
- Validation by confidence function and FCB
- For GPS, QZSS and Galileo (no GLONASS)

AR-OFF



AR-ON



Numerically Stable EKF

Measurement Update of EKF

$$\mathbf{K} = \mathbf{P}^- \mathbf{H}^T (\mathbf{H} \mathbf{P}^- \mathbf{H}^T + \mathbf{R})^{-1}$$

$$\mathbf{x}^+ = \mathbf{x}^- + \mathbf{K}(\mathbf{y} - \mathbf{h}(\mathbf{x}^-))$$

$$\mathbf{P}^+ = (\mathbf{I} - \mathbf{K} \mathbf{H}) \mathbf{P}^-$$

Standard EKF

- (1) $\mathbf{v} = \mathbf{y} - \mathbf{h}(\mathbf{x})$, $\mathbf{H}$, $\mathbf{R}$
- (2) $\mathbf{D} = \mathbf{P} \mathbf{H}^T$ (sparse)
- (3) $\mathbf{S} = \mathbf{H} \mathbf{D} + \mathbf{R}$ (sparse)
- (4) $\mathbf{U} = \text{chol}(\mathbf{S})$ DPOTRF
- (5) $\mathbf{K} = (\mathbf{D} \mathbf{U}^{-1}) \mathbf{U}^{-T}$ DTRSM
- (6) $\mathbf{x} = \mathbf{x} + \mathbf{K} \mathbf{v}$ DGEMV
- (7) $\mathbf{P} = \mathbf{P} - \mathbf{K} \mathbf{D}^T$ DGEMM

Numerically Stable EKF

- (1) $\mathbf{v} = \mathbf{y} - \mathbf{h}(\mathbf{x})$, $\mathbf{H}$, $\mathbf{R}$
- (2) $\mathbf{D} = \mathbf{P} \mathbf{H}^T$ (sparse)
- (3) $\mathbf{S} = \mathbf{H} \mathbf{D} + \mathbf{R}$ (sparse)
- (4) $\mathbf{U} = \text{chol}(\mathbf{S})$ DPOTRF
- (5) $\mathbf{E} = \mathbf{D} \mathbf{U}^{-1}$ DTRSM
- (6) $\mathbf{K} = \mathbf{E} \mathbf{U}^{-T}$ DTRSM
- (7) $\mathbf{x} = \mathbf{x} + \mathbf{K} \mathbf{v}$ DGEMV
- (8) $\mathbf{P} = \mathbf{P} - \mathbf{E} \mathbf{E}^T$ DSYRK

GPS Orbit Quality by MADOCA

IGS AC	Analysis Software	# of Stas	GPS Orbit RMS (cm)				Clock (ns)	
			R	A	C	3D	STD	RMS
	MADOCA 0.3.0	77	0.89	1.10	1.12	1.81	0.109	0.131
ESA	NAPEOS 3.5	110	0.97	1.33	1.09	1.98	0.116	0.183
CODE	Bernese 5.1	231	1.01	1.36	1.14	2.04	0.075	0.089
NGS	arc, orb, pages, gpscom	199	0.95	1.46	1.41	2.24	-	-
GFZ	EPOS.PV2	191	1.15	1.64	1.59	2.56	0.146	0.169
MIT	GAMIT 10.33, GLOBK 5.16	263	1.37	2.12	1.39	2.88	0.277	0.316
NRCan	GIPSY/OASIS-II 5.0	91	2.58	1.72	1.77	3.57	0.128	0.148
JPL	GIPSY/OASIS-II 5.0	142	2.62	1.67	1.98	3.68	0.168	0.226
SIO	GAMIT 10.20, GLOBK 5.08	258	2.42	2.26	1.77	3.75	-	-
GRG	GINs, DYNAMO	134	2.47	2.80	1.74	4.12	0.172	0.212

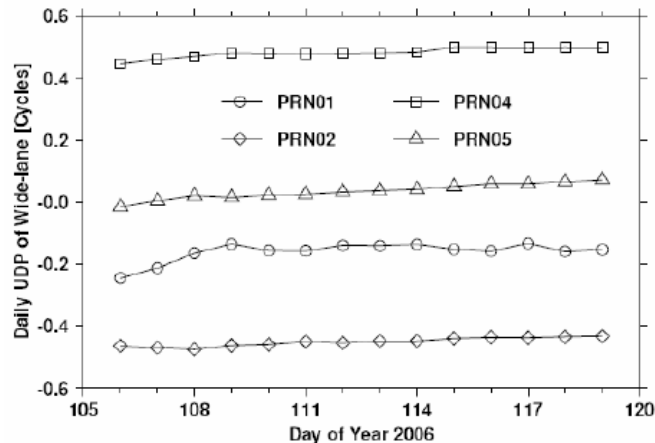
2011/01/01 -2011/12/31 (365 days), wrt IGS Final

Ambiguity Resolution in PPP

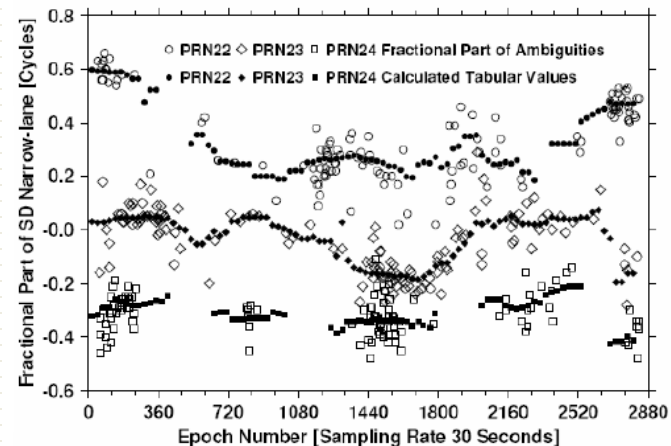
- **with AR for PPP**
 - Improve Convergence Time
 - Improve Accuracy of Static Solution (EW, UD)
 - Improve Stability of Kinematic Solution
- **Difficulties of AR for PPP**
 - Unknown Satellite Initial Phase Biases
 - Effect of Precise Orbit/Clock Error
 - Effect of Ionospheric Delay
 - Code/Phase Bias Instability
 - Multipath Effect at Reference Station Network

M.Ge et al., EGU 2007

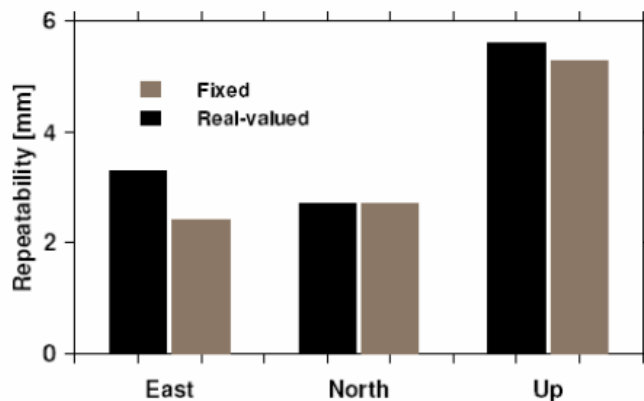
WL Phase Bias Stability



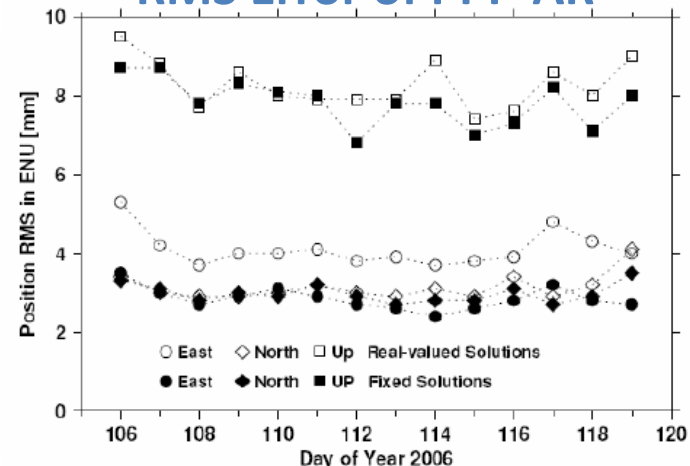
NL Phase Bias Stability



Repeatability of PPP-AR



RMS Error of PPP-AR



M.Ge et al., Resolution of GPS carrier-phase ambiguity in precise point positioning, EGU Assembly 2007

D.Laurichesse, ION 2010

- **Real-Time Implementation of PPP-AR**
 - Network WL ambiguity fixing
 - Parameter estimation by EKF with iono-free code/phase: phase-clock, code-phase-bias, ZTD, station position, orbit correction to IGU, phase ambiguity
 - Orbit construction + high-rate clock generation
- **Evaluation of Accuracy**
 - Orbit: 4cm, code-clock: 5 cm, phase-clock: 1cm
- **RT-PPP with AR ("CNES Integer PPP")**
 - 1 cm HRMS

Future Precise Positioning

	Requirement	Technologies in 2020
Coverage	Global (world-wide)	RT-Orbit/Clock with AR, Broadcast via Internet + GEO/QZSS Satellite
Dynamics	Stationary - Space	Static - Kinematic
Accuracy	1 cm (HRMS) 2 cm (VRMS)	Local iono/tropos corrections (land) Ionos estimation by triple-freq (sea)
Availability	99 % (open sky)	30 sats + triple-freq
	95 % (urban)	30 sats+INS-aided PLL, slip-resistant
Latency	1 s	Real-time corrections
TTFF	10 s (land)	Local iono/tropos corrections
	1 min (sea)	Ionos estimation by triple-freq
User Cost	< \$100	No patent problem, need killer-AP