

For JAXA R&D

PPP - Models, Algorithms and Implementations (4)



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PPP - Models, Algorithms and Implementation

1. 2019-10-04 **PPP models**
geometric range, ionosphere, troposphere, antenna PCV,
earth tides, wind-up, relativity, biases, coordinates
2. 2019-10-18 **PPP algorithms**
SPP, LSQ, GN, EKF, noise-model, RAIM/QC, LAPACK/BLAS
3. 2019-11-01 **PPP data handling**
LC, interpolation, slip detection, RINEX, SP3, ANTEX, RTCM,
CSSR
4. 2019-11-22 **PPP-AR**
UPD/FCB, EWL/WL/NL, ILS, LAMBDA, TCAR, PAR, validation
5. 2019-12-06 **INS integration**
INS sensors, Inertial navigation, INS integration
6. 2019-12-20 **POD of satellites**
orbit element, orbit model, reduced-dynamic,
ECI-ECEF transformation, precession/nutation, EOP

(1.5 h / session)

Notations

c	: Speed of light (m/s)	I_r^s	: Ionospheric delay (m)
P_{r,L_i}^s	: L_i Pseudorange measurement (m)	T_r^s	: Tropospheric delay (m)
φ_{r,L_i}^s	: L_i Carrier phase measurement (cyc)	f_i	: L_i carrier frequency (Hz)
Φ_{r,L_i}^s	: L_i Phase-range measurement (m)	λ_i	: L_i carrier wavelength (m)
t_r	: Signal reception time (s)	B_{r,L_i}^s	: L_i Carrier phase bias (m)
t^s	: Signal transmission time (s)	N_{r,L_i}^s	: L_i Carrier phase ambiguity (cyc)
ρ_r^s	: Geometric range (m)	ε_p	: Code measurement error (m)
$\mathbf{r}^s(t)$: Satellite position in ECEF (m)	ε_Φ	: Phase measurement error (m)
$\mathbf{v}^s(t)$: Satellite velocity in ECEF (m)	ω_e	: Earth rotation velocity (rad/s)
\mathbf{r}_r	: Receiver position in ECEF (m)	Z_t	: Zenith total delay (m)
\mathbf{e}_r^s	: LOS vector in ECEF	Z_h	: Zenith hydrostatic delay (m)
$\mathbf{e}_{r,\text{enu}}^s$: LOS vector in local coordinates	Z_w	: Zenith wet delay (m)
ϕ_r	: Latitude of receiver position (rad)	$m_h(\text{El})$: Hydrostatic mapping function
λ_r	: Longitude of receiver position (rad)	$m_w(\text{El})$: Wet mapping function
h_r	: Ellipsoidal height of receiver (m)	$\mathbf{U}(t)$: ECEF to ECI transformation matrix
H_r	: Orthometric height of receiver (m)	\mathbf{E}_r	: ECEF to local coordinates rotation matrix
Az_r^s	: Azimuth angle of satellite (rad)	\mathbf{E}^s	: ECEF to satellite body rotation matrix
EI_r^s	: Elevation angle of satellite (rad)	$\mathbf{R}_x(\theta)$: Coordinates rotation matrix around X
dt_r	: Receiver clock bias (s)	$\mathbf{R}_y(\theta)$: Coordinates rotation matrix around Y
$dT^s(t)$: Satellite clock bias (s)	$\mathbf{R}_z(\theta)$: Coordinates rotation matrix around Z

Ambiguity Resolution (AR)

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Objectives of AR

- More accurate solutions after proper AR (FIXED vs. FLOAT)
- Faster solution convergence, ideally FIXED instantaneously
- Carrier phase observables can be handled as precise pseudorange after AR

Initial phase terms should be eliminated for AR

- Both of satellite and receiver initial phases do not have integer nature
- DD (double difference) used for baseline processing like RTK

ZD (zero-difference) carrier-phase

$$\Phi_r^s = \rho_r^s + c(dt_r - dT^s(t^s)) - I_r^s + T_r^s + d_r^s + \lambda d_{pw} + \lambda(\phi_{r,0} - \phi_0^s + N_r^s) + \varepsilon_\Phi$$

DD (double-difference) carrier-phase for baseline processing

$$\Phi_{rb}^{ij} = \rho_{rb}^{ij} - I_{rb}^{ij} + T_{rb}^{ij} + d_{rb}^{ij} + \lambda d_{pw,rb}^{ij} + \lambda N_{rb}^{ij} + \varepsilon_\Phi$$

$$\Phi_{rb}^{ij} \approx \rho_{rb}^{ij} + \lambda N_{rb}^{ij} + \varepsilon_\Phi \quad (\text{short-baseline, same antenna})$$

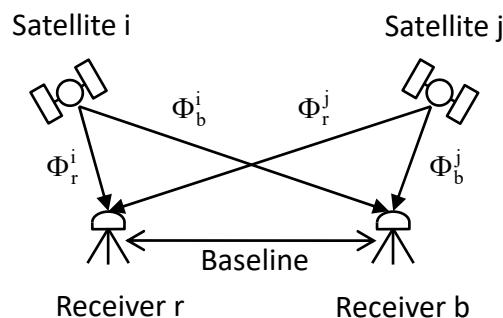
ρ^{ij} : Difference between satellite i and j

ρ_{rb} : Difference between receiver r and b

N_r^s : Integer ambiguity (cyc)

ϕ_0^s : Satellite initial phase (cyc)

$\phi_{r,0}$: Receiver initial phase (cyc)



FIXED Solution with AR

Typical AR Steps [1]

$$(1) \quad \mathbf{y} = \mathbf{Hx} + \boldsymbol{\varepsilon} = \mathbf{Aa} + \mathbf{Bb} + \boldsymbol{\varepsilon} \quad (\mathbf{a} \in \mathbf{Z}^n, \mathbf{b} \in \mathbf{R}^p) \quad \text{Mixed-integer measurement models}$$

$$(2) \quad \hat{\mathbf{x}} = \begin{pmatrix} \hat{\mathbf{a}} \\ \hat{\mathbf{b}} \end{pmatrix}, \mathbf{Q}_{\hat{\mathbf{x}}} = \begin{pmatrix} \mathbf{Q}_{\hat{\mathbf{a}}} & \mathbf{Q}_{\hat{\mathbf{a}}\hat{\mathbf{b}}} \\ \mathbf{Q}_{\hat{\mathbf{b}}\hat{\mathbf{a}}} & \mathbf{Q}_{\hat{\mathbf{b}}} \end{pmatrix} \quad \text{FLOAT solution and VC matrix by LSE or KF}$$

$$(3) \quad \hat{\mathbf{a}} \rightarrow \check{\mathbf{a}} \quad \text{Mapping FLOAT to FIXED}$$

$$(4) \quad \check{\mathbf{b}} = \hat{\mathbf{b}} - \mathbf{Q}_{\hat{\mathbf{b}}\hat{\mathbf{a}}} \mathbf{Q}_{\hat{\mathbf{a}}}^{-1}(\hat{\mathbf{a}} - \check{\mathbf{a}}) \quad \text{FIXED solution}$$

Mapping FLOAT to FIXED ($\hat{\mathbf{a}} \rightarrow \check{\mathbf{a}}$)

Integer Rounding (IR)

$$\check{\mathbf{a}} = [\check{a}] = ([\hat{a}_1], [\hat{a}_2], \dots, [\hat{a}_n])^T$$

Integer Bootstrapping (conditional sequential rounding) (IB)

$$\check{\mathbf{a}} = \left([\hat{a}_1], [\hat{a}_2 - \sigma_{21}\sigma_1^{-2}(\hat{a}_1 - \check{a}_1)], \dots, [\hat{a}_n - \sum_{i=1}^{n-1} \sigma_{n,i|I}\sigma_{i|I}^{-2}(\hat{a}_{i|I} - \check{a}_i)] \right)^T$$

Integer Least Squares (ILS)

$$\check{\mathbf{a}} = \arg \min_{\mathbf{a} \in \mathbf{Z}} (\hat{\mathbf{a}} - \mathbf{a})^T \mathbf{Q}_{\hat{\mathbf{a}}}^{-1} (\hat{\mathbf{a}} - \mathbf{a})$$

\mathbf{a} : Integer ambiguity parameters

\mathbf{b} : Other parameters

$\hat{\mathbf{a}}, \hat{\mathbf{b}}$: FLOAT solutions

$\check{\mathbf{a}}, \check{\mathbf{b}}$: FIXED solutions

$[x]$: Rounding to the nearest integer

$$\mathbf{Q}_{\hat{\mathbf{a}}} = \begin{pmatrix} \sigma_1^2 & \sigma_{12} & \cdots & \sigma_{1n} \\ \sigma_{21} & \sigma_2^2 & \cdots & \sigma_{2n} \\ \vdots & \vdots & \ddots & \vdots \\ \sigma_{n1} & \sigma_{n2} & \cdots & \sigma_n^2 \end{pmatrix}$$

[1] P. J. G. Teunissen and O. Montenbruck (eds.), Springer Handbook of Global Navigation Satellite Systems, 2017, Springer, Section 23

AR by ILS

AR Techniques based on ILS^[1]

Technique	Reference	Ambiguity Search Method	Data Processing Method	Search Space Handling Method	Note
LSAST	Hatch, 1990	Independent	Single-epoch	None	Least-Squares Ambiguity Search Technique
FARA	Frei and Beutler, 1990	All	Multi-epoch	Conditional	Fast Ambiguity Resolution Approach
Modified Cholesky Decomposition	Euler and Landau, 1992	All	Multi-epoch	None	
LAMBDA	Teunissen, 1994	All	Multi-epoch	Transformation/ Conditional	Least-squares AMBiguity Decorrelation Adjustment
Null Space	Martin-Neira, 1995	Independent	Single-epoch	Transformation	
FASF	Chen and Lachapelle, 1995	All	Multi-epoch	Conditional	Fast Ambiguity Search Filter
OMEGA	Kim and Langley, 1999	Independent	Single/ Multi-epoch	Transformation/ Conditional	Optimal Method for Estimating GPS Ambiguities

[1] D. Kim and B. Langley, GPS Ambiguity Resolution and Validation: Methodologies, Trends and Issues, 7th Workshop International Symposium on GPS/GNSS, 2000

LAMBDA

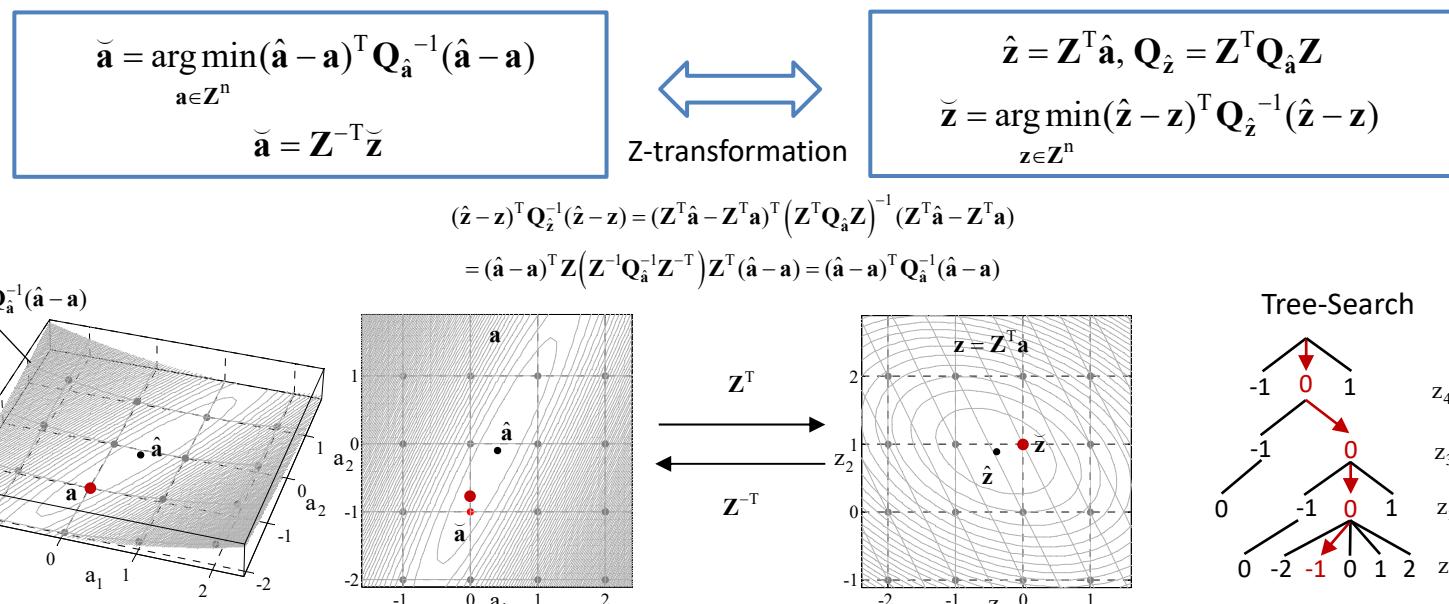
Least-squares AMBiguity Decorrelation Adjustment [1]

A GNSS AR strategy by ILS estimator

Shrinking integer search space with "decorrelation"

Skillful and efficient tree search strategy

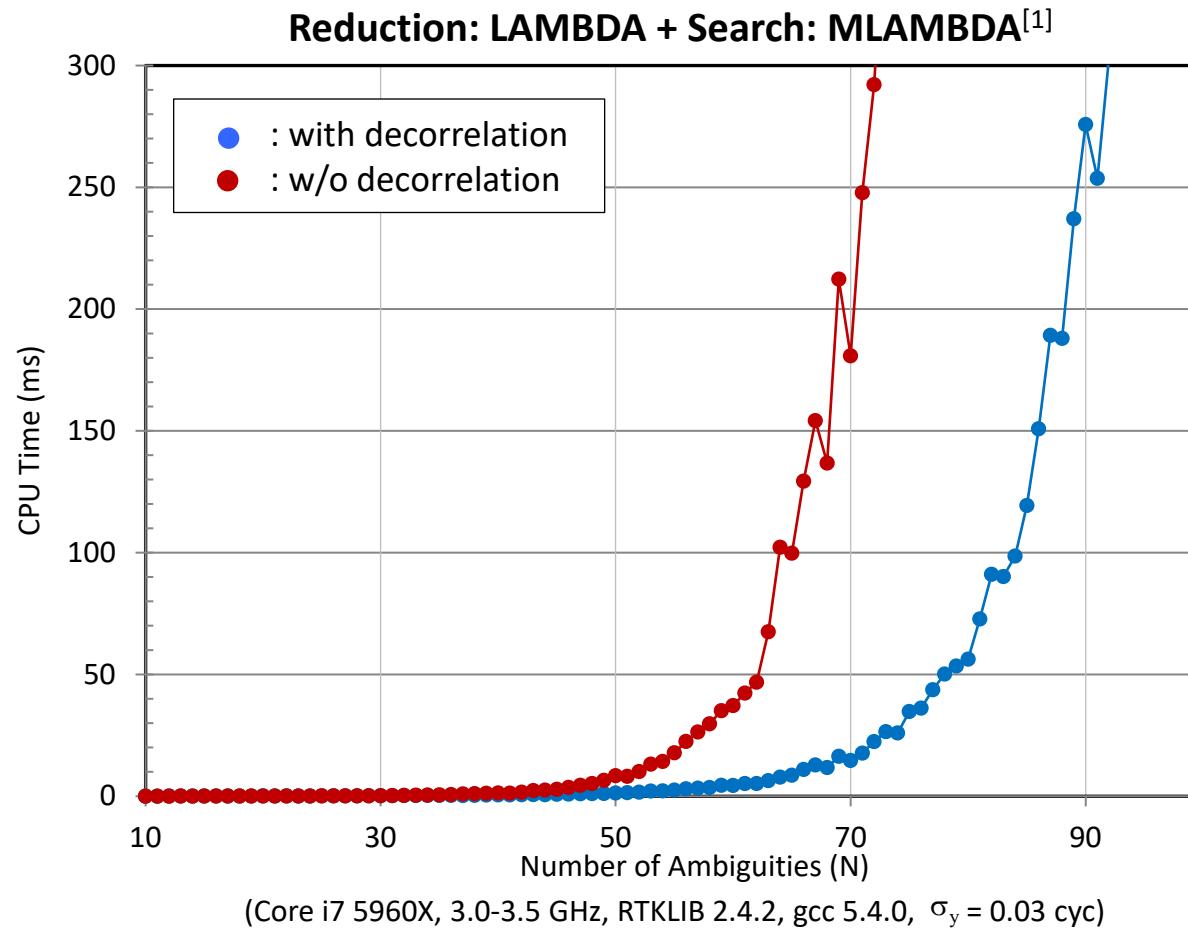
Similar to "Closest Point Search with LLL Lattice Basis Reduction" Algorithm [2]



[1] P. J. G. Teunissen, The least-squares ambiguity decorrelation adjustment: a method for fast GPS integer ambiguity estimation. *Journal of Geodesy*, 1994

[2] E. Agrell, Closest point search in lattices, *IEEE Transaction on Information Theory*, 2002

CPU Time for LAMBDA



[1] X. -W. Chang, X. Yang and T. Zhou, MLAMBDA: A modified LAMBDA method for integer least-squares estimation, Journal of Geodesy, 2005

Validation of AR

Acceptance Test after AR

Wrong AR much degrades the quality of the final (FIXED) solution

Need to maximize AR success probability and to minimize AR failure rate

Remain ambiguities FLOAT if the acceptance test failed and output FLOAT solution instead

Several acceptance tests are proposed: [1]

Ratio Test

$$\text{accept } \check{\mathbf{a}} \text{ if : } \frac{\|\hat{\mathbf{a}} - \check{\mathbf{a}}'\|_{Q_{\hat{\mathbf{a}}}}^2}{\|\hat{\mathbf{a}} - \check{\mathbf{a}}\|_{Q_{\hat{\mathbf{a}}}}^2} \geq c$$

Difference Test

$$\text{accept } \check{\mathbf{a}} \text{ if : } \|\hat{\mathbf{a}} - \check{\mathbf{a}}'\|_{Q_{\hat{\mathbf{a}}}}^2 - \|\hat{\mathbf{a}} - \check{\mathbf{a}}\|_{Q_{\hat{\mathbf{a}}}}^2 \geq c$$

F-Ratio Test

$$\text{accept } \check{\mathbf{a}} \text{ if : } \frac{\|\hat{\mathbf{e}}\|_{Q_y}^2 + \|\hat{\mathbf{a}} - \check{\mathbf{a}}'\|_{Q_{\hat{\mathbf{a}}}}^2}{\|\hat{\mathbf{e}}\|_{Q_y}^2 + \|\hat{\mathbf{a}} - \check{\mathbf{a}}\|_{Q_{\hat{\mathbf{a}}}}^2} \geq c$$

Projector Test

$$\text{accept } \check{\mathbf{a}} \text{ if : } \left| \frac{(\check{\mathbf{a}}' - \check{\mathbf{a}})^T Q_{\hat{\mathbf{a}}}^{-1} (\hat{\mathbf{a}} - \check{\mathbf{a}})}{\|\check{\mathbf{a}}' - \check{\mathbf{a}}\|_{Q_{\hat{\mathbf{a}}}}^2} \right| \leq \mu$$

$\check{\mathbf{a}}'$: Second-best candidate of AR, c, μ : Test thresholds $\|x\|_Q^2 = x^T Q^{-1} x$ $\hat{\mathbf{e}} = \mathbf{y} - \mathbf{A}\hat{\mathbf{a}} - \mathbf{B}\hat{\mathbf{b}}$

Note: The test thresholds are usually selected empirically as a fixed value (for example Ratio Test with $c = 3$). The threshold value, however, is often optimistic or conservative without theoretical basis.
In some literatures, variable threshold values are proposed base on fixed-failure rate approach (FF-RT) [2].

[1] S. Verhagen and P. J. G. Teunissen, New global navigation satellite system ambiguity resolution method compared to exiting approaches, Journal of Guidance, Control and Dynamics, 2006

[2] S. Verhagen and P. J. G. Teunissen, The ratio test for future GNSS ambiguity resolution, GPS Solution, 2013

Partial AR (PAR)

Partial AR (PAR)

Full AR (FAR) indicates low fixing ratio or long TTFF under ill conditions like long BL RTK

Newly rising satellites or cycle-slips often disturbs FAR with validation

Degraded accuracy by PAR solutions acceptable in many applications

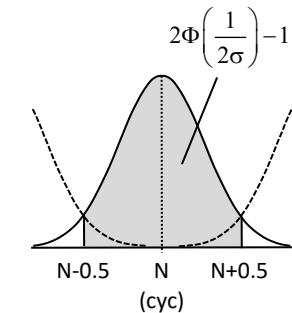
Many criteria how to select subset of ambiguities:

Elevation angle, continuous tracking epochs, SNR, ADOP (ambiguity dilution of precision), EWL/WL/NL, success or failure probability of AR

BSR (bootstrapping success rate) Criterion [1]

$$\prod_{i=k}^n \left(2\Phi\left(\frac{1}{2\sigma_{\hat{z}_{i|I}}}\right) - 1 \right) \geq P_0$$

P_0 : Minimum success probability of bootstrapping AR
 $\sigma_{\hat{z}_{i|I}}$: Std-dev of Z-transformed i-th ambiguity of bootstrapping AR
 $\Phi(x)$: CDF (cumulative distribution function) of normal distribution



FF-RT (fixed-failure-rate ratio-test) Criterion [1]

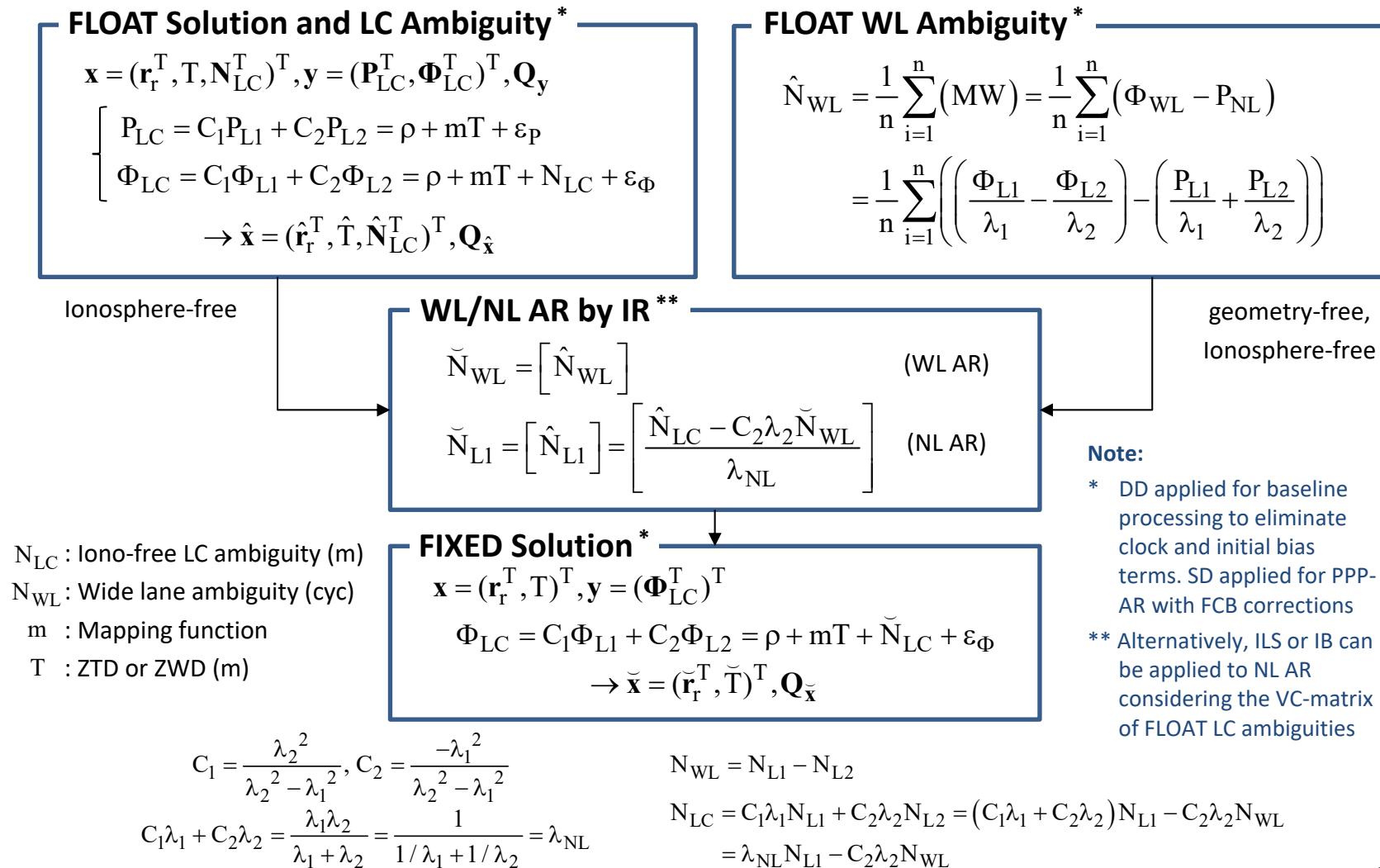
$$\frac{\|\hat{\mathbf{z}}_p - \check{\mathbf{z}}'_p\|_{Q_{\hat{\mathbf{z}}_p}}^2}{\|\hat{\mathbf{z}}_p - \check{\mathbf{z}}_p\|_{Q_{\hat{\mathbf{z}}_p}}^2} \geq c(n, P_f)$$

$p = (k, k+1, \dots, n)$: Partial set of Z-transformed ambiguities
 $\hat{\mathbf{z}}_p$: Float Z-transformed ambiguities
 $\check{\mathbf{z}}_p, \check{\mathbf{z}}'_p$: Best-fixed, secondary-best-fixed Z-transformed ambiguities
 $c(n, P_f)$: Threshold of FF-RT (fixed-failure-rate ratio-test)

$$\begin{aligned} \Phi(x) &= \frac{1}{\sqrt{2\pi}} \int_{-\infty}^x \exp\left(-\frac{t^2}{2}\right) dt \\ &= \frac{1}{2} \left(1 - \operatorname{erf}\left(\frac{x}{\sqrt{2}}\right) \right) \end{aligned}$$

[1] S. Verhagen et al., GNSS ambiguity resolution: which subset to fix ?, International GNSS Symposium, 2011

WL/NL AR with Iono-free LC



L1/L2 AR with STEC Estimation

FLOAT Solution, STEC and L1/L2 Ambiguity * ***

$$\mathbf{x} = (\mathbf{R}^T, \mathbf{N}^T)^T, \mathbf{y} = (\mathbf{P}_{L1}^T, \mathbf{P}_{L2}^T, \boldsymbol{\Phi}_{L1}^T, \boldsymbol{\Phi}_{L2}^T)^T, \mathbf{Q}_y$$

$$\begin{cases} P_{L1} = \rho + I + mT + \varepsilon_P \\ P_{L2} = \rho + \gamma I + mT + \varepsilon_P \\ \Phi_{L1} = \rho - I + mT + \lambda_1 N_{L1} + \varepsilon_\Phi \\ \Phi_{L2} = \rho - \gamma I + mT + \lambda_2 N_{L2} + \varepsilon_\Phi \end{cases} \quad \begin{pmatrix} \mathbf{R} = (\mathbf{r}_r^T, T, \mathbf{I}^T)^T \\ \mathbf{N} = (\mathbf{N}_{L1}^T, \mathbf{N}_{L2}^T)^T \end{pmatrix}$$

$$\rightarrow \hat{\mathbf{x}} = (\hat{\mathbf{R}}^T, \hat{\mathbf{N}}^T)^T, \mathbf{Q}_{\hat{\mathbf{x}}} = \begin{pmatrix} \mathbf{Q}_{\hat{\mathbf{R}}} & \mathbf{Q}_{\hat{\mathbf{N}}\hat{\mathbf{R}}} \\ \mathbf{Q}_{\hat{\mathbf{R}}\hat{\mathbf{N}}} & \mathbf{Q}_{\hat{\mathbf{N}}} \end{pmatrix}$$

L1/L2 AR by ILS **

$$\breve{\mathbf{N}} = \arg \min_{\mathbf{N} \in \mathbf{Z}^n} (\hat{\mathbf{N}} - \mathbf{N})^T \mathbf{Q}_{\hat{\mathbf{N}}}^{-1} (\hat{\mathbf{N}} - \mathbf{N})$$

FIXED Solution

$$\breve{\mathbf{R}} = (\breve{\mathbf{r}}_r^T, \breve{T}, \breve{\mathbf{I}}^T)^T = \hat{\mathbf{R}} - \mathbf{Q}_{\hat{\mathbf{R}}\hat{\mathbf{N}}} \mathbf{Q}_{\hat{\mathbf{N}}}^{-1} (\hat{\mathbf{N}} - \breve{\mathbf{N}})$$

I : Slant ionospheric delay (STEC) at L1 frequency (m) $\gamma = (\lambda_2 / \lambda_1)^2$

Note:

- * DD applied for baseline processing to eliminate clock and initial bias terms. SD applied for PPP-AR with FCB corrections

- ** PAR instead of FAR could be applied to improve fixing ratio and TTFF

- *** It is easily enhanced to triple or quad frequency measurements

TCAR/CIR

TCAR (three-carrier AR) [1] /CIR (cascade integer resolution) [2]

Sequential conditional rounding EWL -> WL -> NL ambiguities

Geometry-free measurement model

Ionosphere terms can be reduced by short baseline or ionosphere corrections (for PPP)

Many modifications or enhancements including geometry-based models

$$(1) \check{N}_{EWL} = \left[\frac{\Phi_{EWL} - P_X}{\lambda_{EWL}} \right]$$

$$(2) \check{N}_{WL} = \left[\frac{\Phi_{WL} - (\Phi_{EWL} - \lambda_{EWL} \check{N}_{EWL})}{\lambda_{WL}} \right]$$

$$(3) \check{N}_{NL} = \left[\frac{\Phi_{NL} - (\Phi_{WL} - \hat{N}_{WL})}{\lambda_{NL}} \right]$$

$$\begin{cases} P_X = \rho + I_X + T + \epsilon_P \\ \Phi_{EWL} = \rho - I_{EWL} + T + \lambda_{EWL} N_{EWL} + \epsilon_{\Phi_{EWL}} \\ \Phi_{WL} = \rho - I_{WL} + T + \lambda_{WL} N_{WL} + \epsilon_{\Phi_{WL}} \\ \Phi_{NL} = \rho - I_{NL} + T + \lambda_{NL} N_{NL} + \epsilon_{\Phi_{NL}} \end{cases}$$

$$|I_X + I_{EWL}| \ll \lambda_{EWL}, |I_{WL}| \ll \lambda_{WL}, |I_{NL}| \ll \lambda_{NL}$$

Typical Selection of EWL, WL and NL for GPS

$$P_X = \frac{P_{L2}/\lambda_2 + P_{L5}/\lambda_5}{1/\lambda_2 + 1/\lambda_5}, \Phi_{EWL} = \frac{\Phi_{L2}/\lambda_2 - \Phi_{L5}/\lambda_5}{1/\lambda_2 - 1/\lambda_5}, \Phi_{WL} = \frac{\Phi_{L1}/\lambda_1 - \Phi_{L2}/\lambda_2}{1/\lambda_1 - 1/\lambda_2}, \Phi_{NL} = \Phi_{L1}$$

[1] U. Vollath et al., Analysis of three-carrier ambiguity resolution (TCAR) technique for precise relative positioning in GNSS-2, ION GPS-98

[2] J. Jung and P. Enge, Optimization of cascade integer resolution with three civil GPS frequency, ION GPS 2000

Triple Frequency LC

$$\Phi_{(i,j,k)} = \frac{i/\lambda_1 \Phi_{L1} + j/\lambda_2 \Phi_{L2} + k/\lambda_5 \Phi_{L5}}{i/\lambda_1 + j/\lambda_2 + k/\lambda_5} \quad P_{(l,m,n)} = \frac{l/\lambda_1 P_{L1} + m/\lambda_2 P_{L2} + n/\lambda_5 P_{L5}}{l/\lambda_1 + m/\lambda_2 + n/\lambda_5}$$

Type	LC	Coefficients						λ_{LC} (cm)	I_{LC} (wrt P1)	σ_{LC}		Note
		i	j	k	l	m	n			(cm)	(cyc)	
Geometry Based	$\Phi_{(1,0,0)}$	1	-	-	-	-	-	19.0	-1	0.3	0.016	NL
	$\Phi_{(0,1,0)}$	-	1	-	-	-	-	24.4	-1.647	0.3	0.012	NL
	$\Phi_{(0,0,1)}$	-	-	1	-	-	-	25.5	-1.793	0.3	0.012	NL
	$\Phi_{(1,-1,0)}$	1	-1	-	-	-	-	86.1	1.283	1.7	0.020	WL
	$\Phi_{(1,0,-1)}$	1	-	-1	-	-	-	75.1	1.339	1.5	0.020	WL
	$\Phi_{(0,1,-1)}$	-	1	-1	-	-	-	586.1	1.719	10.0	0.017	EWL
	$\Phi_{(1,-6,5)}$	1	-6	5	-	-	-	325.6	0.074	31.1	0.096	EWL
	$\Phi_{(1,-5,4)}$	1	-5	4	-	-	-	209.3	0.662	16.5	0.079	EWL
	$\Phi_{(4,-3,0)}$	4	-3	-	-	-	-	11.4	-0.090	0.8	0.073	NL
	$\Phi_{(4,0,-3)}$	4	-	-3	-	-	-	10.8	0.010	0.8	0.072	NL
Geometry Free	$\Phi_{(1,-1,0)} - P_{(1,1,0)}$	1	-1	-	1	1	-	86.1	0	21.4	0.249	WL
	$\Phi_{(1,0,-1)} - P_{(1,0,1)}$	1	-	-1	1	-	1	75.1	0	21.5	0.286	WL
	$\Phi_{(0,1,-1)} - P_{(0,1,1)}$	-	1	-1	-	1	1	586.1	0	23.4	0.040	EWL
	$\Phi_{(1,-6,5)} - P_{(1,1,1)}$	1	-6	5	1	1	1	325.6	-1.360	35.7	0.110	EWL
	$\Phi_{(1,-6,5)} - P_{(1,1,0)}$	1	-6	5	1	1	-	325.6	-1.209	37.8	0.116	EWL
	$\Phi_{(1,-5,4)} - P_{(1,1,1)}$	1	-5	4	1	1	1	209.3	-0.773	24.1	0.115	EWL
	$\Phi_{(1,-5,4)} - P_{(1,1,0)}$	1	-5	4	1	1	-	209.3	-0.622	27.0	0.129	EWL

$$\lambda_{LC} = \frac{1}{i/\lambda_1 + j/\lambda_2 + k/\lambda_5} \quad N_{LC} = i \cdot N_{L1} + j \cdot N_{L2} + k \cdot N_{L5} \quad I_{LC} = -\frac{i/\lambda_1 + j/\lambda_2/\lambda_1^2 + k/\lambda_5/\lambda_1^2}{i/\lambda_1 + j/\lambda_2 + k/\lambda_5} - \frac{1/\lambda_1 + m/\lambda_2/\lambda_1^2 + n/\lambda_5/\lambda_1^2}{1/\lambda_1 + m/\lambda_2 + n/\lambda_5}$$

$$\sigma_{LC} = \sqrt{\frac{(i/\lambda_1)^2 + (j/\lambda_2)^2 + (k/\lambda_5)^2}{(i/\lambda_1 + j/\lambda_2 + k/\lambda_5)^2} \sigma_\Phi^2 + \frac{(l/\lambda_1)^2 + (m/\lambda_2)^2 + (n/\lambda_5)^2}{(l/\lambda_1 + m/\lambda_2 + n/\lambda_5)^2} \sigma_p^2} \quad (\sigma_\Phi = 0.3 \text{ cm}, \sigma_p = 30 \text{ cm})$$

PPP-AR

PPP-AR

PPP (w/o AR)

Developed by JPL in 1990s to facilitate the analysis of large reference station N/W data [1]

Conventionally PP (post processing) with IGS precise ephemeris

AR has been difficult due to unknown satellite initial phase term

$$\Phi_r^s = \rho_r^s + c(dt_r - dT^s(t^s)) - I_r^s + T_r^s + d_r^s + \lambda d_{pw} + \lambda(\phi_{r,0} - \phi_0^s + N_r^s) + \varepsilon_\Phi$$

Satellite initial phase

PPP-AR (PPP with AR)

Many research works have been done to introduce AR for PPP

- Based on FCB (fractional cycle bias) or UPD (uncalibrated phase delay) [2]
- Based on IRC (integer recovery clock) or decoupled clock model [3]
- Based on globally estimated phase ambiguities in reference station N/W [4]

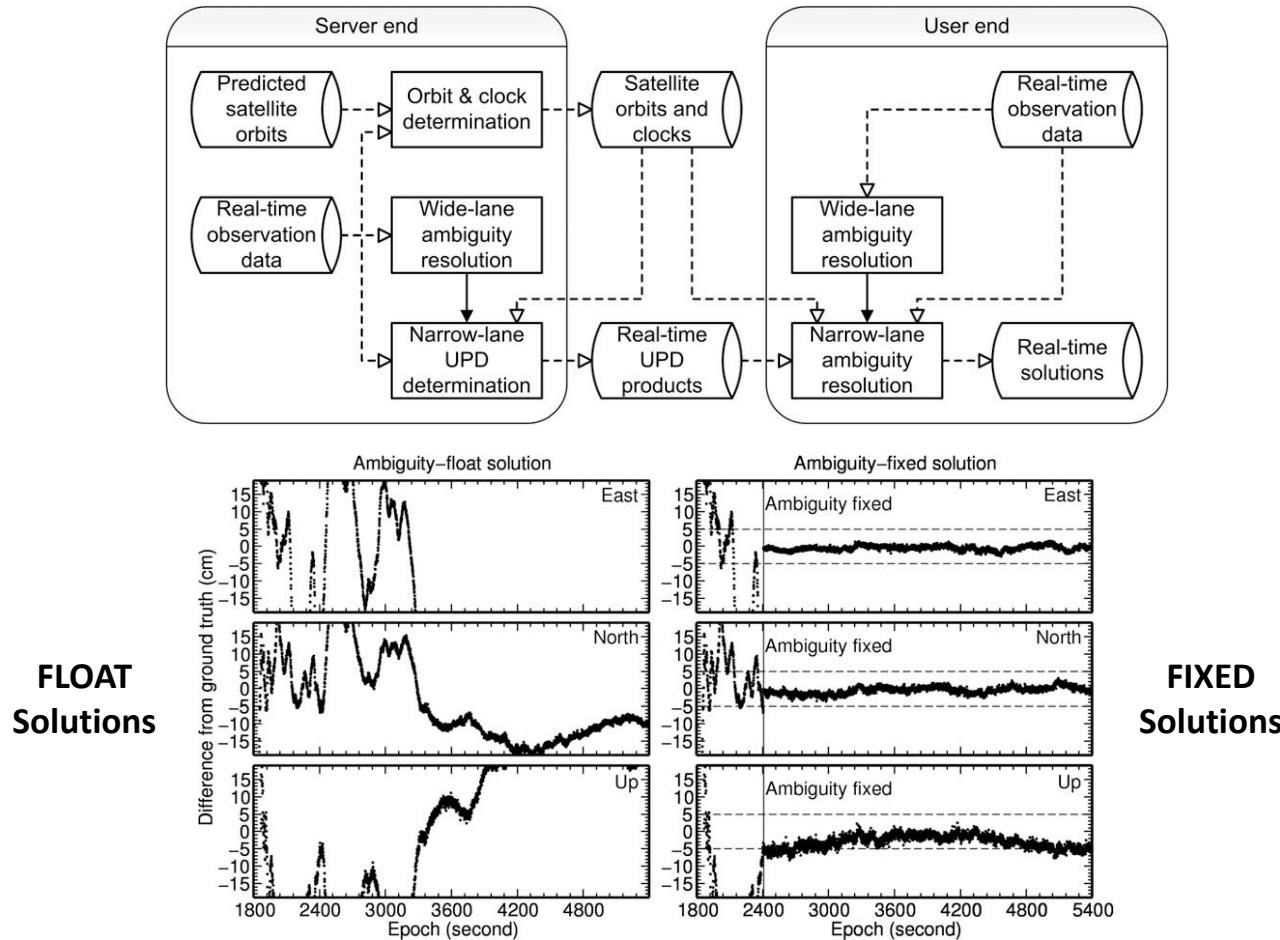
Recently PPP-AR is enhanced to RT (real-time) [5] and multi-constellation GNSS

Commercial PPP Services based on PPP-AR

Several services have been already launched since 2000s

- [1] J. F. Zumberge et al., Precise Point Positioning for the efficient and robust analysis of GPS data from large networks, *Journal of Geophysical Research*, 1997
- [2] M. Ge et al., Resolution of GPS carrier-phase ambiguities in Precise Point Positioning (PPP) with daily observation, *Journal of Geodesy*, 2008
- [3] P. Collins et al., Precise Point Positioning with ambiguity resolution using the decoupled clock model, *ION ITM* 2008
- [4] W. Bertiger et al., Single receiver phase ambiguity resolution with GPS data, *Journal of Geodesy*, 2010
- [5] D. Laurichesse et al., Real time-difference ambiguities fixing and absolute RTK, *ION NTM* 2008

RT PPP-AR



- [1] J. Geng et al., Towards PPP-RTK: Ambiguity resolution in real-time precise point positioning, *Advances in Space Research*, 2010

FCB/UPD Generation

Generate SD-Ambiguity

$$\hat{B}_{k,XL}^{i,j} = (\hat{B}_{k,XL}^i - \hat{B}_{k,XL}^j) / \lambda_{XL}$$

Average SD-FCB (A)

$$b_{XL}^{i,j} = \frac{1}{n} \sum_{k=1}^n \left((\hat{B}_{k,XL}^{i,j} - b_0) - [(\hat{B}_{k,XL}^{i,j} - b_0)] \right) + b_0$$

FCB SD-to-ZD Decomposition

$$\mathbf{b}_{SD} = (b_{XL}^{1,2}, \dots, b_{XL}^{1,m}, b_{XL}^{2,3}, \dots, b_{XL}^{2,m}, \dots, b_{XL}^{m-1,m})^T$$

$$\mathbf{b}_{ZD} = (b_{XL}^1, b_{XL}^2, \dots, b_{XL}^m)^T = \left((\mathbf{D}^T, \mathbf{1}) (\mathbf{D}^T, \mathbf{1})^T \right)^{-1} (\mathbf{D}^T, \mathbf{1}) (\mathbf{b}_{SD}^T, \mathbf{0})^T$$

FCB Validation

$$N = \hat{B}_{k,XL}^{i,j} - (b_{XL}^i - b_{XL}^j)$$

if $|N - [N]| > \delta N_{max}$ or $P_N(N, \sigma_B) < P_{N,min}$, reject $\hat{B}_{k,XL}^{i,j}$ and goto (A), end

NL/WL/EWL -> L1/L2/L5 [1]

$$b_{L1}^i = b_{NL}^i - b_{WL}^i \cdot \lambda_1 / (\lambda_2 - \lambda_1)$$

$$b_{L2}^i = b_{NL}^i - b_{WL}^i \cdot \lambda_2 / (\lambda_2 - \lambda_1)$$

$$b_{L5}^i = b_{L2}^i - b_{EWL}^i$$

XL : Ambiguity type (NL/WL/EWL/L1/2/5)

i, j : Satellite

k : Receiver in ref stations N/W

$\hat{B}_{k,XL}^i$: Estimated float ambiguity (m)

$\hat{N}_{k,XL}^{i,j}$: SD-float ambiguity (cyc)

$b_{XL}^{i,j}$: SD-FCB (cyc)

b_{XL}^i : ZD-FCB (cyc)

b_0 : Initial SD-FCB (cyc)

D : ZD to SD transformation matrix

$$(\mathbf{b}_{SD} = \mathbf{D}\mathbf{b}_{ZD})$$

Orbit/Clock Generation

NL/WL/EWL Ambiguity

Generate SD-Ambiguity

Average SD-EWL-FCB

EWL-FCB SD-to-ZD Decom.

EWL-FCB Validation

Average SD-WL-FCB

WL-FCB SD-to-ZD Decom.

WL-FCB Validation

Average SD-NL-FCB

NL-FCB SD-to-ZD Decom.

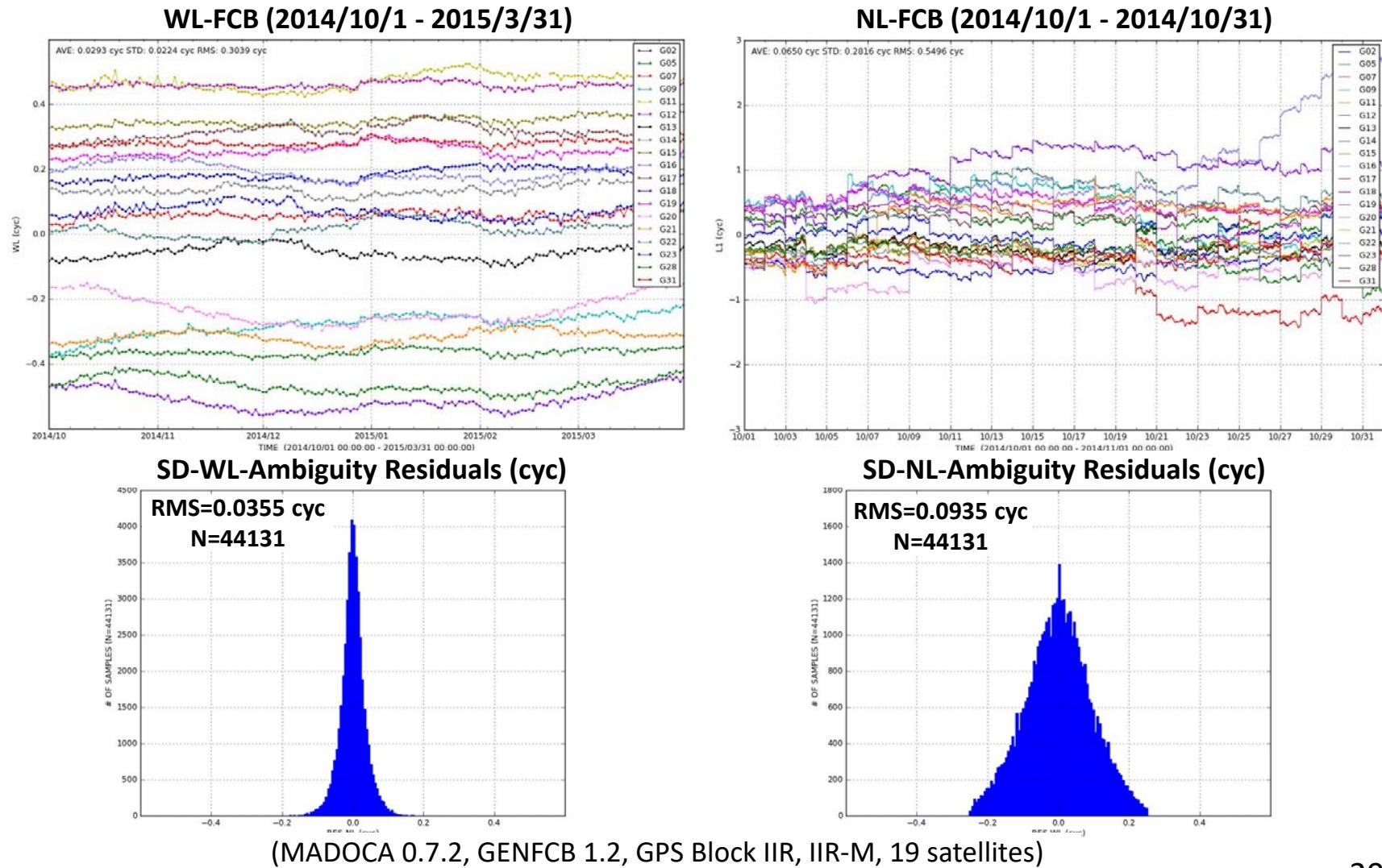
NL-FCB Validation

NL/WL/EWL -> L1/L2/L5

L1/L2/L5 FCB Products

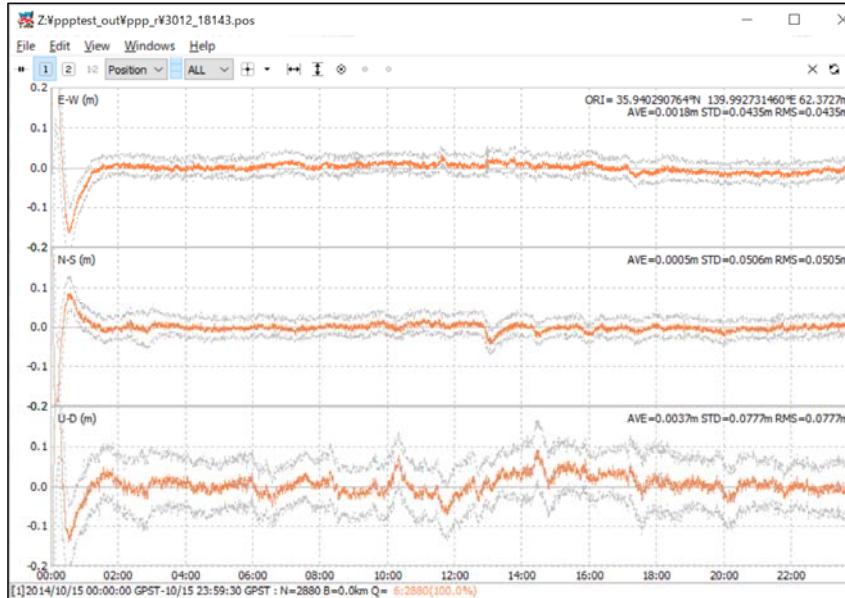
[1] X. Li et al., A method for improving uncalibrated phase delay estimation and ambiguity-fixing in real-time precise point positioning, Journal of Geodesy, 2013

FCB/UPD Examples



PPP-AR Example

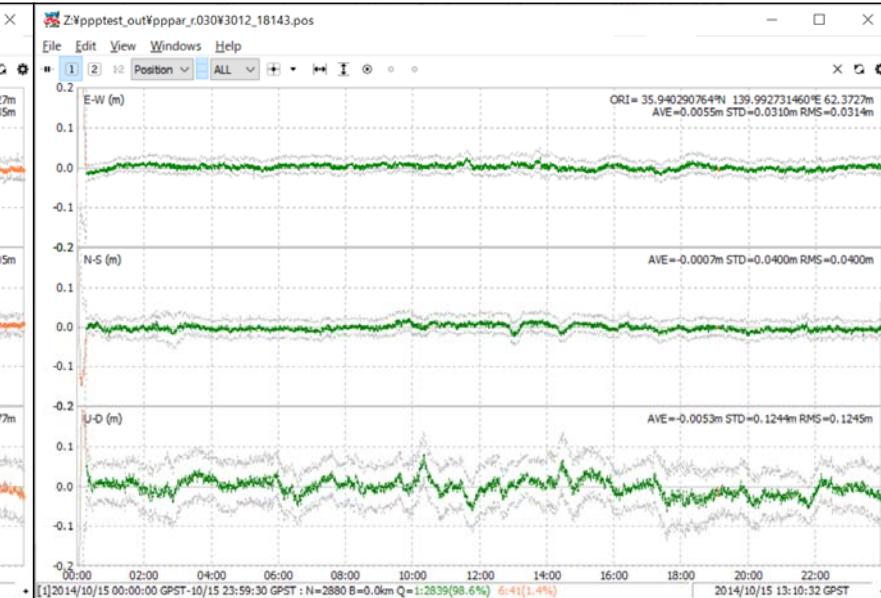
PPP (w/o AR)



RMS Error: E 1.01, N 0.77, U 2.29 cm

(Kinematic mode, First 1 H solutions excluded for convergence time)

PPP-AR



RMS Error: E 0.67, N 0.72, U 2.02 cm

● FLOAT ● FIXED

(MADOC 0.7.2, GENFCB 1.2, RTKLIB 2.4.2, GEONET 3012, 2014/10/15 0:00:00-23:59:30 GPST)

Commercial PPP Services

Service	Provider	Supported GNSS	# of Ref. Stations	Comm. Link	Receivers	Accuracy
StarFire™ [1]	 NAVCOM A John Deere Company (US)	GPS, GLO	> 40	3 GEO (L-band), IP	NavCom	< 5 cm
Seastar™ [2]	 FUGRO (NED)	GPS, GLO, GAL, BDS (G4)	~ 80	6 GEO (L-band), IP (NTRIP)	Fugro	10 cm H 15 cm V (95%)
Apex/Ultra [3] TerraStar® [4]	 veripos  (UK)	GPS, GLO, GAL, BDS, QZS (Apex ⁵)	~ 80	7 GEO (L-band)	VERIPOS, NovAtel ^[7] , Septentrio ^[8] , TOPCON ^[9] , Hemisphere ^[10]	< 5 cm H < 12 cm V (95%)
CenterPoint RTX [5]	 Trimble (US)	GPS, GLO, GAL, BDS, QZS	~ 100	6 GEO (L-band), IP (NTRIP)	Trimble, Qualcomm (?)	2 cm H 5 cm V (RMS)
magicGNSS [6]	 gmv INNOVATING SOLUTIONS (Spain)	GPS, GLO, GAL, BDS, QZS	~ 80	IP (NTRIP)	(RTCM SSR)	5 cm H 8 cm V (RMS)
GEOFLEX [11]	 geo flex (France)	GPS, GLO, (GAL, BDS)	~ 100	GEO, IP, GPRS/UMTS	(RTCM SSR)	4 cm (2D-95%)

[1] <https://www.navcomtech.com>, [2] <https://www.fugro.com>, [3] <https://veripos.com>, [4] <https://www.terrastar.net>,

[5] <https://positioningservices.trimble.com>, [6] <https://magicgnss.gmv.com>, [7] <https://www.notavel.com>,

[8] <https://www.septentrio.com>, [9] <https://www.topconpositioning.com>, [10] <https://www.hemispherengnss.com>,

[11] <http://www.geoflex.fr>

PPP Service Performance

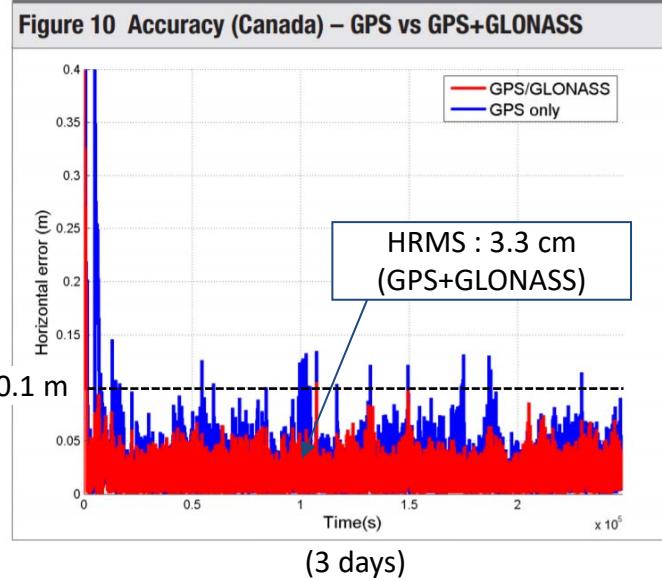


Table 5: Error Statistics at the Canada Station

PPP Correction Source	Horizontal RMS Error (cm)	Vertical RMS Error (cm)
TerraStar-C (GPS/GLONASS)	3.3	4.9
TerraStar-C (GPS only)	4.4	6.5

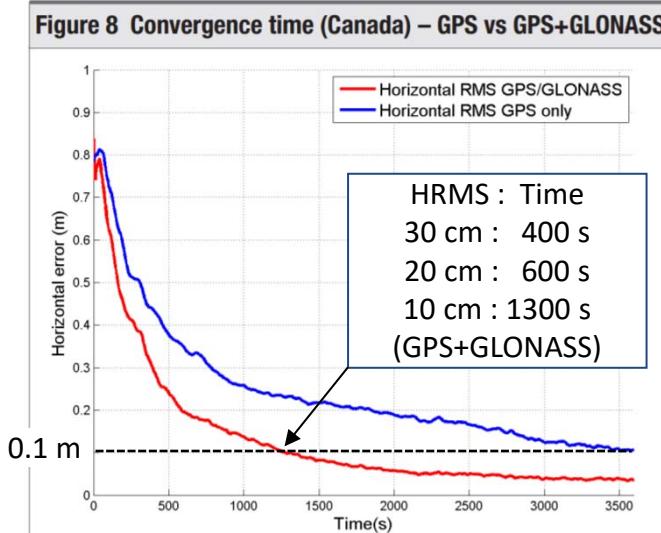
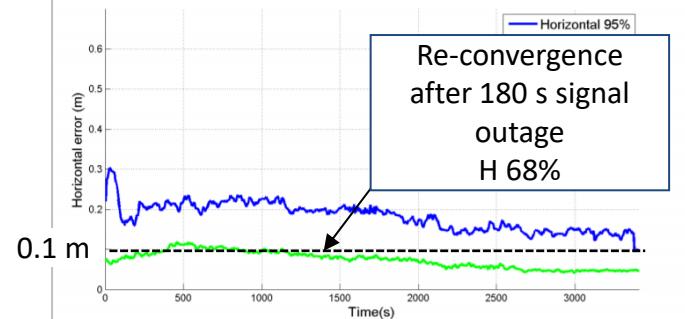


Figure 6 Re-convergence after 180 second signal outage



(NovAtel Correct with TerraStar-C in 2015)

- [1] NovAtel White Paper, Precise Positioning with NovAtel CORRECT Including Performance Analysis, April 2015 (<https://www.novatel.com/assets/Documents/Papers/NovAtel-CORRECT-PPP.pdf>)

Faster Convergence for PPP-AR

PPP-RTK

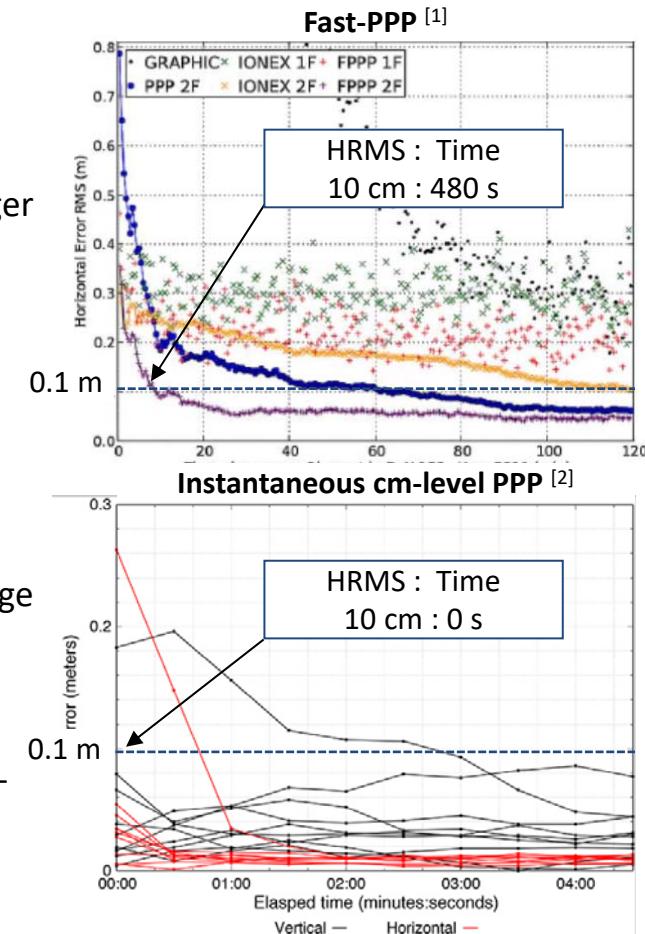
PPP-AR with local STEC and troposphere corrections
High bandwidth required to support broad coverage larger than nation-wide
Dense CORS N/W required for local corrections
Supported by CLAS and some commercial PPP services

Fast-PPP [1]

PPP-AR with global VTEC corrections
Multi-layer model for global VTEC model
Low bandwidth to transmit corrections for global coverage

Instantaneous cm-level PPP [2]

No local or global TEC corrections
Cascading PPP-AR with triple or quad frequencies (L1-L2-L5, E1-E5a-E5b-E6)



[1] A. R. Garcia et al., A worldwide ionospheric model for fast precise point positioning, IEEE Transaction on Geoscience and Remote Sensing, 2015

[2] D. Laurichesse and S. Banville, Innovation: Instantaneous centimeter-level multi-frequency precise point positioning, GPS World, 2018